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Hamilton DIVISION OF UNITED AIRCE Standard

> RESULTS OF PROP-FAN MODEL/STOL WING ACOUSTIC TESTS

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### ABSTRACT

This report summarizes the results of a test conducted to determine the noise characteristics of a STOL wing with externally blown flaps in the vicinity of an aircraft propulsor. The STOL wing used for these tests was a 0.43 scale model with 60° and 0° flap capabilities; however, this wing system was not an optimum configuration, nor was it representative of all STOL wing/flap systems. The propulsor used was a low tip speed, high bypass ratio, low pressure ratio, variable pitch Prop-Fan Model. Far field noise data and directional character were determined for a 60° and 0° flap configuration. In addition, the noise character of the 21 inch diameter Prop-Fan Model without the STOL wing was evaluated.

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### INTRODUCTION

In order to develop information related to the noise characteristics of a model STOL wing with externally blown flaps in the vicinity of an aircraft propulsor, a noise test has been conducted on a Prop-Fan/STOL Wing model at NASA Langley, Hampton, Virginia. The effect of the STOL wing and externally blown flaps on the level and directional character of the noise produced within the fan shroud, and the level and directional character of the noise generated by scrubbing and interaction of the high velocity jet wake from the propulsor with the STOL wing and flaps is discussed in detail.

The model tested consisted of a 0.43 scale STOL wing with flaps set at 60° and 0° mounted aft of a 21 inch diameter, 12 bladed Prop-Fan model with 22 swirl recovery vanes. The Prop-Fan model was originally designed for wind tunnel performance testing and incorporated no noise reduction features except for the use of 22 recovery vanes to suppress the tone level at the blade passing frequency. In this program an existing Prop-Fan test facility was used which precluded optimization of the Prop-Fan/STOL wing system.

The noise tests, which were conducted under controlled free field conditions, included measurements of far field and directional characteristics of the Prop-Fan/STOL Wing model for the 60° flap (setting which would be used during landing of a STOL aircraft), 0° flap (flap retracted flush with the wing surface), and no wing configuration, at various combinations of power (from 72 to 208 HP) and fan tip speeds (from 600 to 800 ft/sec).



## CONCLUSIONS

Based on the results of the Prop-Fan/STOL Wing noise test the following is evident:

- 1. Maximum perceived noise and overall sound pressure propagates at an angle of 40° to 70° from the Prop-Fan exit.
- 2. In the scale of the model tested, the maximum 10 foot flyover noise varies approximately 6.5 dB per doubling of shaft power for both overall SPL and PNL for all wing and flap configurations tested.
- 3. The interaction of the Prop-Fan jet wake with the STOL Wing produced scrubbing noise even with the flaps fully retracted. This is shown by an increase in the low frequency (112 to 449 Hz) noise by as much as 12 dB with the flaps set at 0°. In addition, extending the flaps to 60° increased the level of low frequency noise by as much as 20 dB.
- 4. The STOL Wing with extended flaps increases the measured Prop-Fan 10 foot flyover noise by an average of 3.5 PNdB while the retracted flaps increased the 10 foot flyover noise by an average of 2.8 PNdB.
- 5. The installation of the STOL wing and flaps causes a change in the Prop-Fan tone noise level and directivity.

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# RECOMMENDATIONS

It is recommended that further tests be conducted to determine the effect on noise due to (1) location of the Prop-Fan relative to the wing, (2) direction of fan flow relative to the wing and (3) flap setting.

#### DESCRIPTION OF TEST

#### TEST ITEM

The test item consisted of a 0.43 scale STOL wing model with 60° and 0° externally blown flaps as shown on Figures 1 and 2, mounted above and aft of a 21 inch diameter, 12 bladed, manually adjustable pitch, shrouded Prop-Fan model with 22 fixed pitch recovery vanes. The Prop-Fan rotor, which is shown in Figure 3, was an existing wind tunnel model which was designed for 950 ft/sec tip speed, 400 HP, 0.20 free stream Mach Number and a rotor pressure ratio of 1.110. The recovery vanes were designed to be tested at static conditions at 700 ft/sec tip speed, 222 HP condition. The Prop-Fan shroud was a bellmouth type designed for unseparated inflow during static conditions. The only noise control measure incorporated into the system was the use of 22 stators to promote decay of rotor/stator interaction tone noise. These were located such that the distance between the trailing edge of the rotor blades and the leading edge of the stators was equal to two blade chords at the mean radius. Figure 4 shows the Prop-Fan/STOL Wing installation.

### TEST FACILITY

The tests were conducted on a level grass covered field adjacent to Building 1212 at Langley Research Center, Hampton, Virginia. During the test program the Prop-Fan was driven by an electrically powered Propeller Test Rig (PTR) normally used for aerodynamic testing in the United Aircraft Wind Tunnel. It should be noted that the installation was such that the Prop-Fan inlet air was drawn over the PTR which is opposite from the installation of Reference 1, which provided a cleaner inflow for Prop-Fan noise evaluation. The axis of rotation was approximately 11.5 feet above the ground and the test area was free from obstructions within 100 feet of the test item. Six far field microphones were located 10 feet from the Prop-Fan, 11.5 feet off the ground, at 22.5 degree intervals. In addition, one microphone was located on a boom capable of traversing continuously from 0-150° on a 10 foot arc as shown in Figure 5. The traversing speed was held in most cases to approximately 0.5° per second.

# INSTRUMENTATION

The following equipment was used for the program:

#### A. Data Acquisition

- 1. Eight Bruel and Kjaer type 4133 microphones with flat response to 40 KHz at normal incidence.
- 2. Eight Bruel and Kjaer type 2614 cathode followers.



- 3. Three Bruel and Kjaer type UA0052 nose cone wind screens.
- 4. Two Bruel and Kjaer model 140 four channel signal conditioners.
- 5. Hewlett Packard model 15117A microphone calibrator providing a 1 KHz signal at 94, 104, 114, or 124 dB ±0.3 dB.
- 6. CEC model VR3300, one inch, 14 channel, direct record tape recorder with a flat response to 40 KHz at 15 inches per second.

#### B. Data Reduction

- 1. General Radio type 1921 one-third octave band real time analyzer.
- 2. Spectral Dynamics type 101 frequency analyzer with stationary and tracking filter capabilities.

#### TEST PROCEDURE

Prior to testing, the microphone and power supplies were allowed to warm up to ensure stability. The microphones were then calibrated using the Hewlett Packard calibrator. This calibration procedure was repeated prior to, and following, each set of tests to determine any calibration shifts that may occur during testing.

To ensure minimum interference from background noise and excessive wind velocities, testing was restricted to the hours between 7 PM and 9 AM. Furthermore, total background noise measurements (ambient and electrical noise) were made at the gain settings used during the test.

Data was recorded for approximately four minutes for each of the appropriate microphone locations in addition to the continuous sweep microphone which traversed approximately 120° at a nominal 0.5 degree/sec for the test conditions of Table 1.



#### DISCUSSION

### INTRODUCTION

In reducing the test data from this program, particular attention was given to determining the effect of the STOL wing and flaps on the internally generated Prop-Fan noise level and directional character as well as the character of noise generated by the jet wake interacting with the wing and flaps. Based on these objectives, the sweep microphone was analyzed with 1/3 octave band filters every 10° of angular travel using a four second averaging time (which minimizes statistical error without obscuring the directional character of the source). This data is tabulated in Appendix A. In addition, selected data were analyzed with a 40 Hz constant bandwidth filter to allow discrimination between tone and broad band noise.

Appendix B contains a discussion of the data accuracy with necessary corrections based on data acquisition/reduction frequency response, microphone frequency response, and total background noise. A summary of test conditions for this program is shown in Table 1 while Table 2 gives the ambient conditions during the test.

#### PERFORMANCE TEST DATA

Prop-Fan thrust (T) and shaft horsepower (SHP) were determined based on the performance information obtained in Reference 1. This data is shown on Figures 6 and 7. It should be noted, however, that no corrections were made to the performance data for the difference in Prop-Fan orientation between this test program and that of Reference 1.

#### ACOUSTIC TEST DATA

Based on the one-third octave band data of Appendix A, the overall sound pressure level (OASPL) on a 10 foot radius was determined for each test condition. The directional character of this data for the "flaps extended," "flaps retracted," and "no wing" configuration for each combination of blade angle and tip speed is shown on Figures 8 through 10. In like manner, the perceived noise level (PNL) as measured on a line 10 feet from, and parallel to, the Prop-Fan axis of rotation (i.e. a 10 foot flyover), is shown on Figures 11 through 13. From these curves it can be seen that both the maximum OASPL and PNL occur 40° to 70° from the Prop-Fan exit for the wing with flaps extended, retracted, and for the no wing configuration. This directional character was further verified by the results of the Prop-Fan model tests described in Reference 1.

These curves also show a significant effect of the wing and flaps on the internally generated Prop-Fan noise as a function of angular location. In general both the OASPL and PNL, which are primarily controlled by the mid-to-high frequency tone and broad band noise produced by the Prop-Fan, are a maximum with the flaps extended. This increase in the measured noise

can be attributed to both an increase in the internally generated acoustic power of the Prop-Fan and reflection of internally generated noise from the STOL wing.

From these data the maximum OASPL on a 10 foot flyover was calculated for each test condition. The results, as shown on Figure 14, follow a trend curve:

$$OASPL_{(MAX)} = 61.6 + 22.7 log SHP \pm 2.5 dB$$

over the horsepower range shown which corresponds to a 6.8 dB increase in OASPL(MAX) per doubling of horsepower. Similarly, Figure 15 shows the maximum PNL on a 10 foot flyover following a trend curve:

$$PNL(MAX) = 78.4 + 21 log SHP \pm 2 dB$$

over the horsepower range shown which corresponds to a 6.3 dB increase per doubling of horsepower.

Both the flap interaction and wing interaction noise (i.e. the difference between the flap extended noise level and no wing noise level and between the flaps retracted noise level and no wing noise level) is shown in Figure 16 for each combination of blade angle and tip speed for the 10 foot-60° microphone location, which generally proved to be the location of maximum noise level. Another view of interaction noise can be obtained by summing the one third octave bands from 125 to 400 Hz for each test configuration as a function of angular position. This is shown in Figures 17 through 19 for each blade angle and tip speed.

Again, selecting the maximum noise location (10 foot-60° microphone location), the effect of the STOL wing and flaps on the entire frequency spectrum is shown in one-third octave bands in Figures 20 through 25. These curves clearly show the low frequency noise below 1 KHz generated by the STOL wing and flap as well as their effect on the Prop-Fan tone noise. It should be noted that the change in tone level due to the STOL wing/flap configuration may be caused by a directivity shift as well as reflection and reinforcement from the wing itself. This can be observed in the erratic directivity pattern of Figure 26 for the fundamental of blade passing frequency.

Narrow band analyses of the 45° blade angle, 683 ft/sec test case as shown on Figures 27 through 29, clearly show the tone content of the noise spectrum due to rotor blade loading (rotor field) and to fluctuating lift on the stators due to wakes from the rotor (rotor/stator interaction). The relatively high fundamental tone, as compared to the data of Reference 1 which showed suppression of the fundamental tone due to the stator count selection can be attributed to the presence of the PTR immediately upstream of the Prop-Fan inlet which prevented the desired uniform inflow conditions. Higher order harmonics, which tend to decrease in level, are clearly evident past the tenth overtone in each case shown.



Further limited analysis of these curves show not only an increase in the low frequency noise floor (interaction noise) due to the presence of the STOL wing and flaps, but also an increase in the broad band noise by as much as 10 dB from 1.5K to 4 KHz and from 9K to 12 KHz.

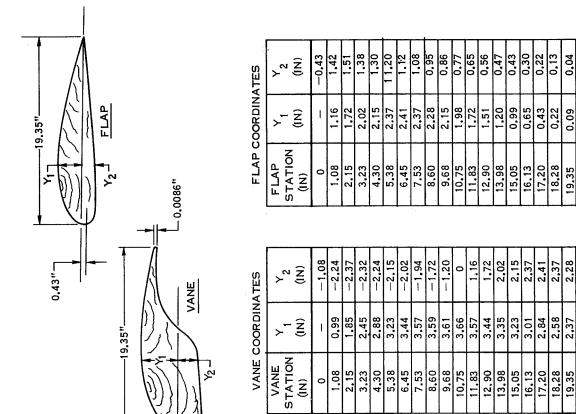
Comparison of the one-third octave band curve with the narrow band curve, as shown in Figure 30 for the 45° blade angle, 683 ft/sec tip speed test condition with flaps extended show the fundamental of blade passing frequency and the first two overtones dominating the noise levels in the respective one-third octave band while the broad band noise floor contributes heavily elsewhere. Therefore, suppression of these tones, which are located in the area of greatest PNL weighting, will significantly aid in reducing perceived noise. This curve also demonstrates the consistency between the two types of analyses.

In order to determine the effect of the Prop-Fan installation (i.e. locating the PTR upstream of the fan) on the overall noise, the test data for the Prop-Fan without the wing was compared to the data of Reference 1 for four similar test cases. The results, as shown on Figures 31 and 32, indicate fair agreement between the two test programs. In general, however, the overall noise is higher for these latest tests, especially at the locations of maximum noise (40°-70° from Prop-Fan exit).



### ACKNOWLEDGMENT

The author wishes to thank Dominic Maglieri, Harry Morgan, and Bob Pegg of NASA Langley Research Center for their invaluable contributions in making this test program possible, supplying the STOL wing model, and assisting in the measurement program.



2.15

1.08

3.23 4.30 5.38

-0.65

6.45 7.53 8.60 9.68

10,75

2.88

3,23

9.88 10.96 12.03

3.44 3,63

3,57

14.18 13,11

15,26 16,33

3.61

1.85 2.45

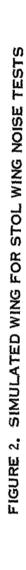
0.99

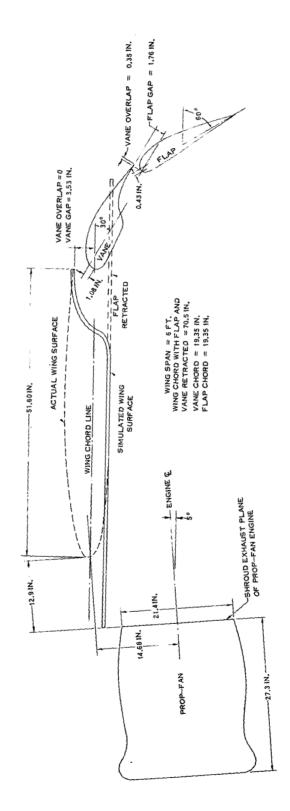
11.83

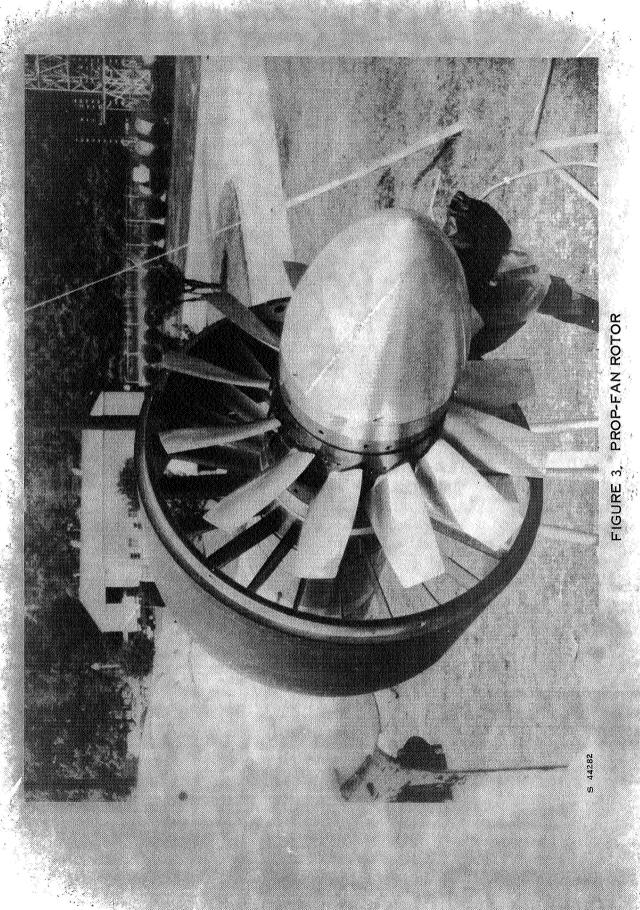
12,90 13,98

15.05 16.13 17.20 18.28 19,35

1.08" -16,33" -2.80-2.82 -2.37-2,67 > <u>≅</u> AFT WING COORDINATES PAST STA.A STA.A STATION 1.28 3.43 4.50 5.58 6.66 7.73 8.81 AFT WING SECTION







o

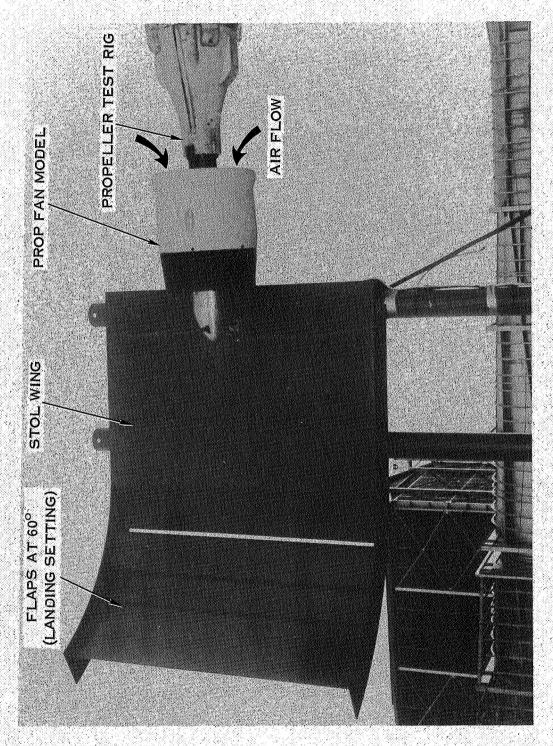


FIGURE 4. PROP-FAN/STOL WING INSTALLATION

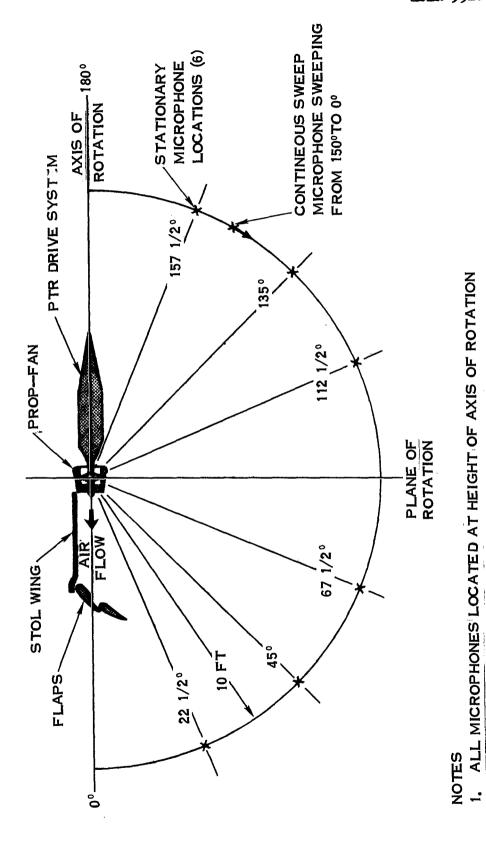


FIGURE 5 PROP-FAN/STOL WING NOISE TEST MICROPHONE LOCATIONS

DRAWING IS NOT TO SCALE

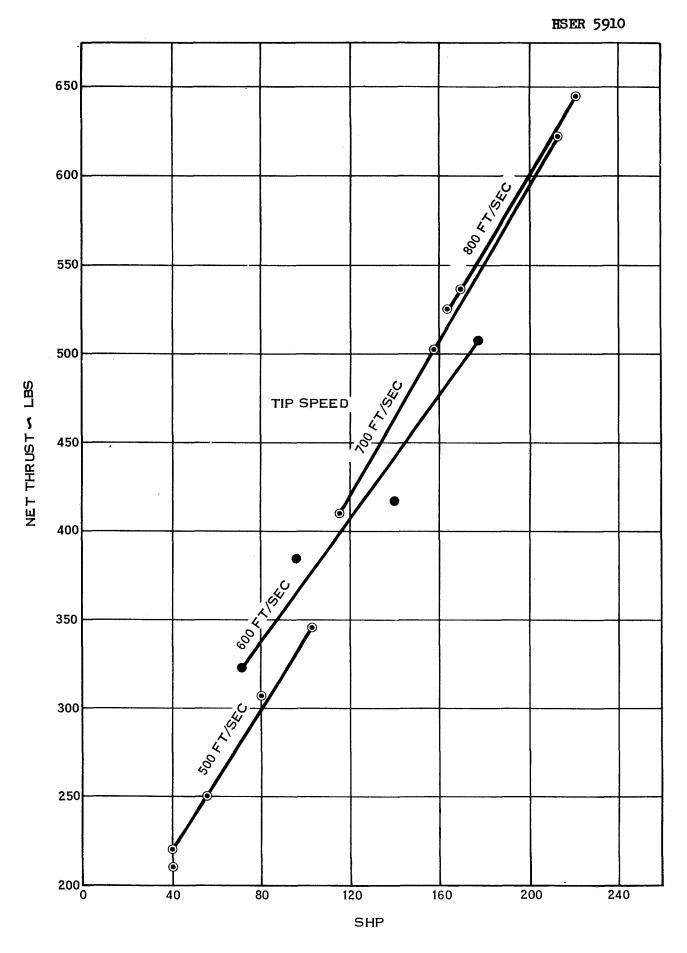


FIGURE 6 PROP-FAN PERFORMANCE

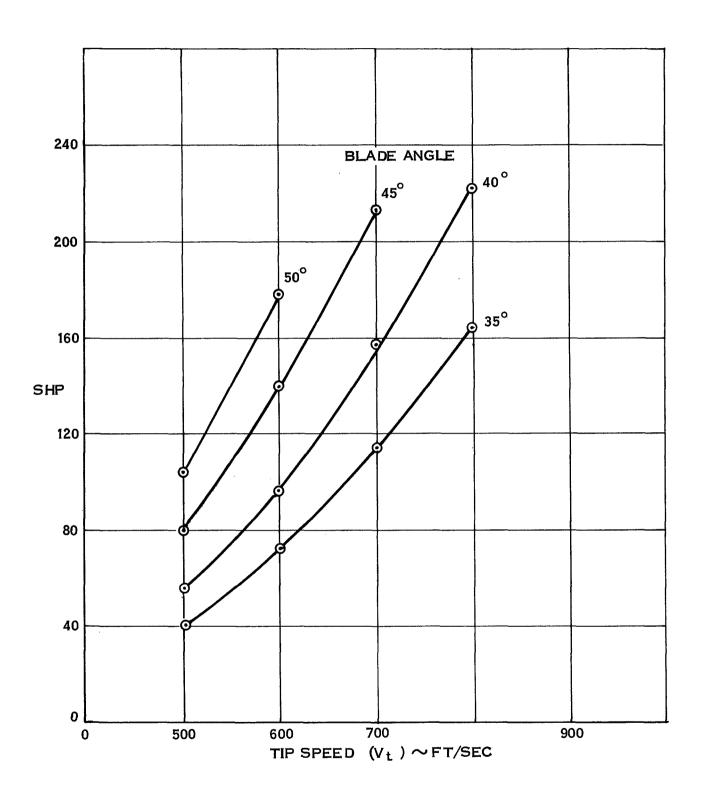
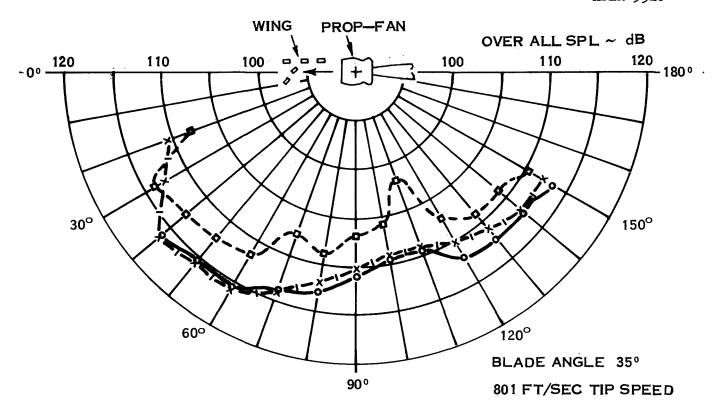


FIGURE 7 PROP—FAN PERFORMANCE



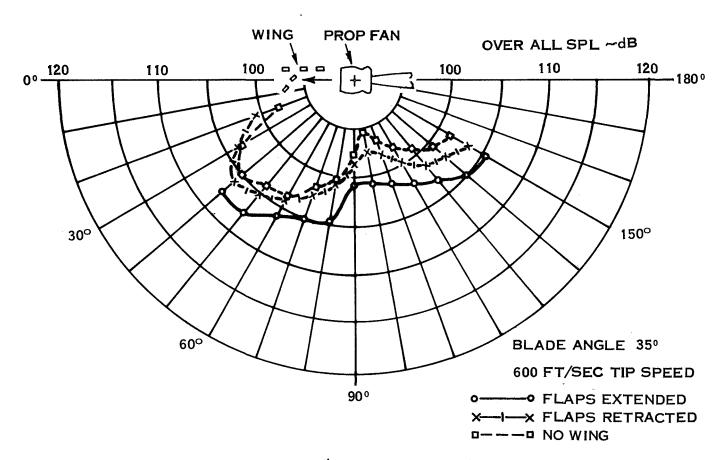
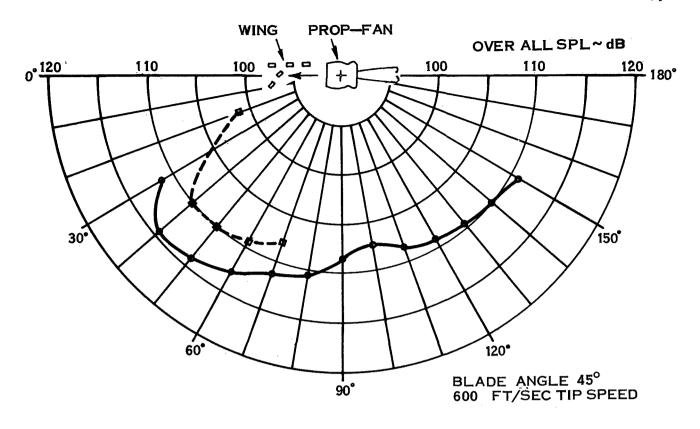


FIGURE 8 PROP-FAN/STOL WING NOISE



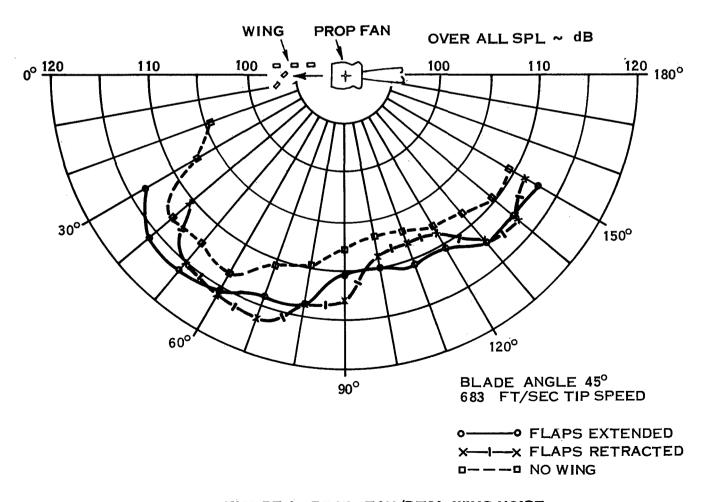
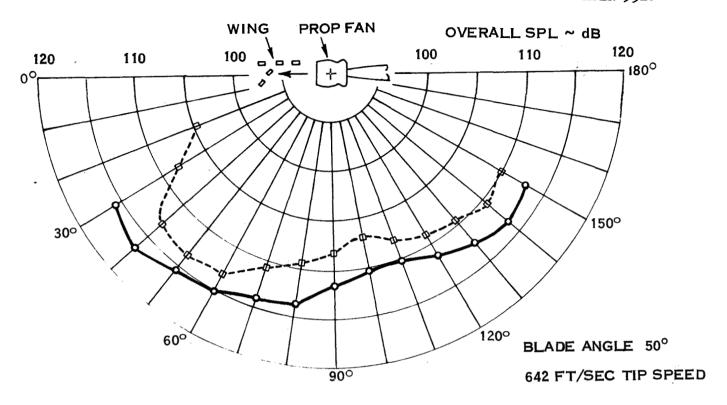


FIGURE 9 PROP-FAN/STOL WING NOISE



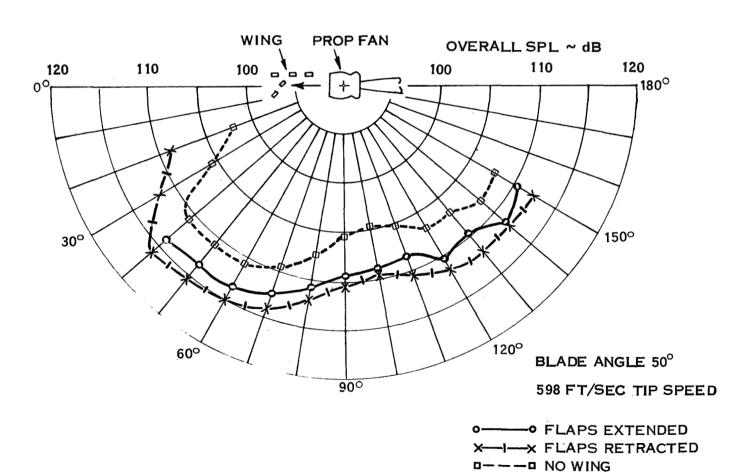
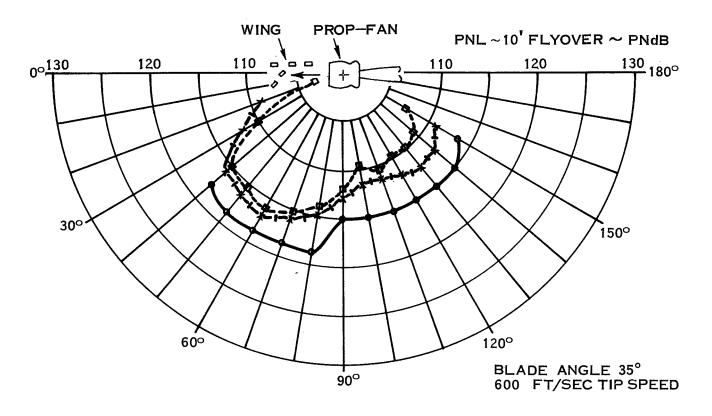
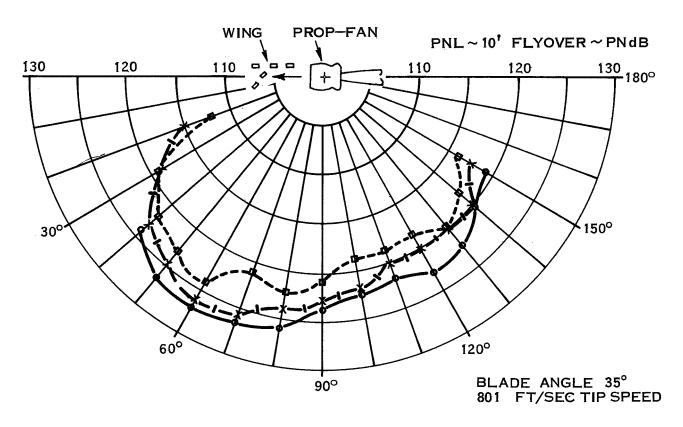


FIGURE 10 PROP-FAN/STOL WING NOISE





•——• FLAPS EXTENDED

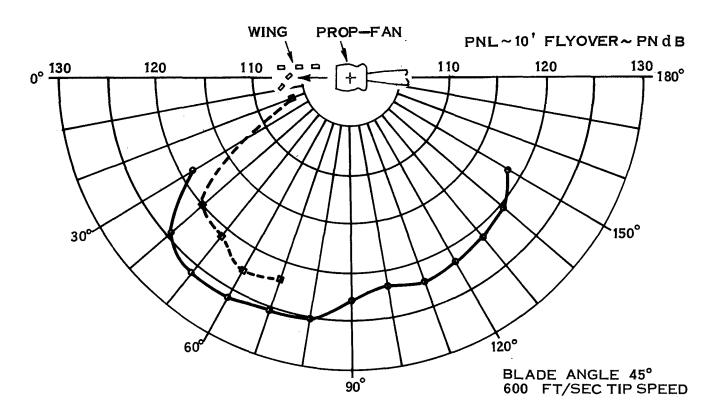
\*——— FLAPS RETRACTED

•——• NO WING

FIGURE 11, PROP—FAN/STOL WING NOISE

PNL ~10 FLYOVER

20



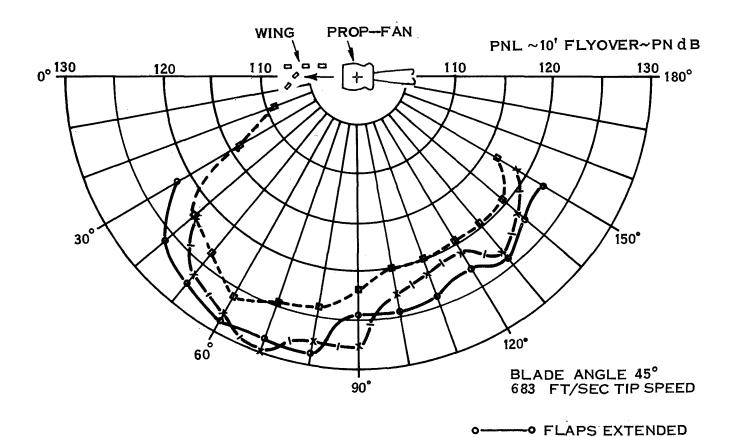
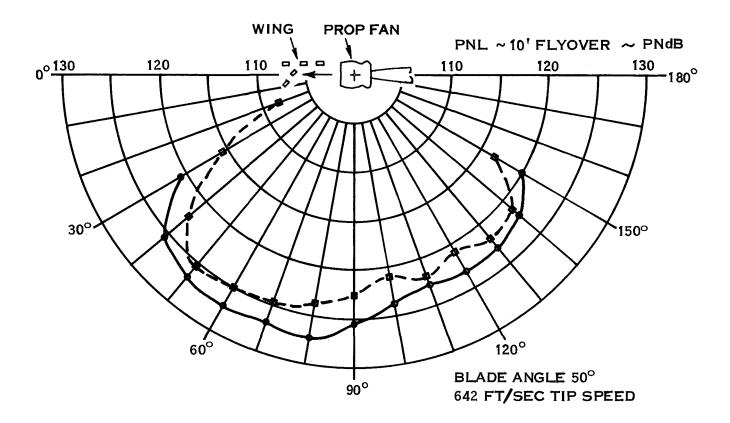


FIGURE 12 PROP—FAN/STOL WING NOISE PNL ~10' FLYOVER

X-I-X FLAPS RETRACTED

--- NO WING



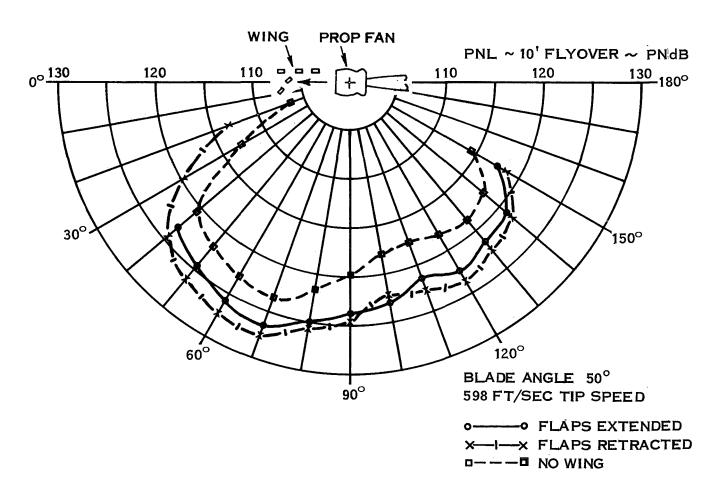
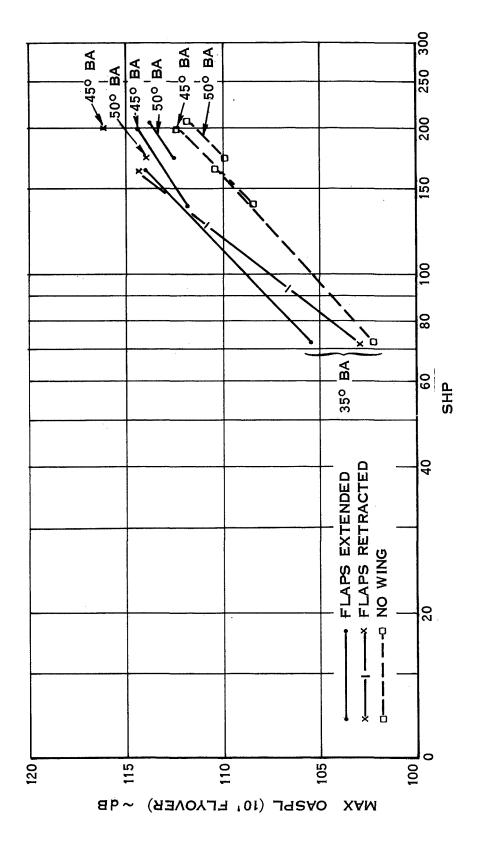


FIGURE 13 PROP—FAN/STOL WING NOISE PNL ~10 FLYOVER



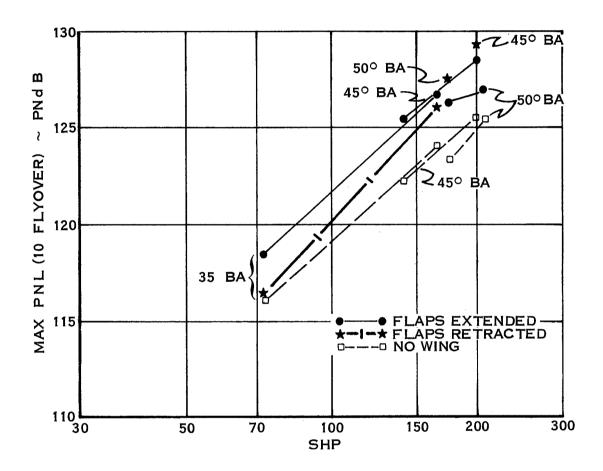
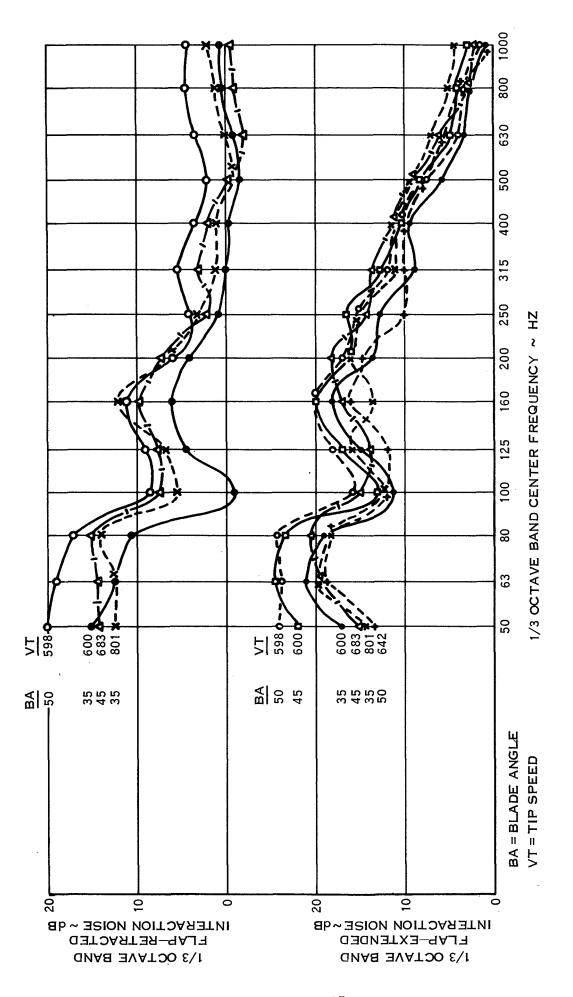
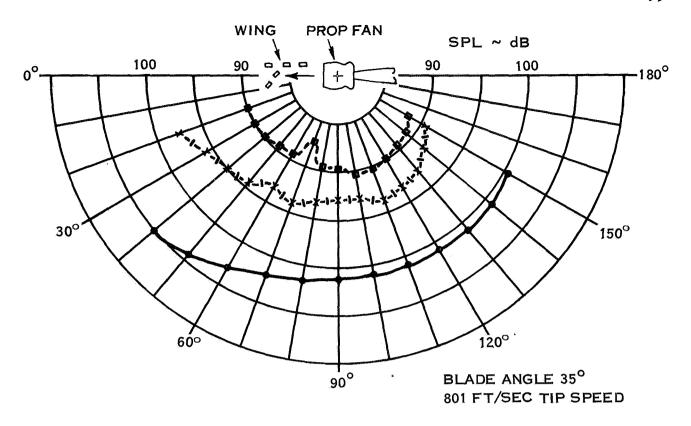


FIGURE 15. PROP-FAN/STOL WING PERCEIVED NOISE





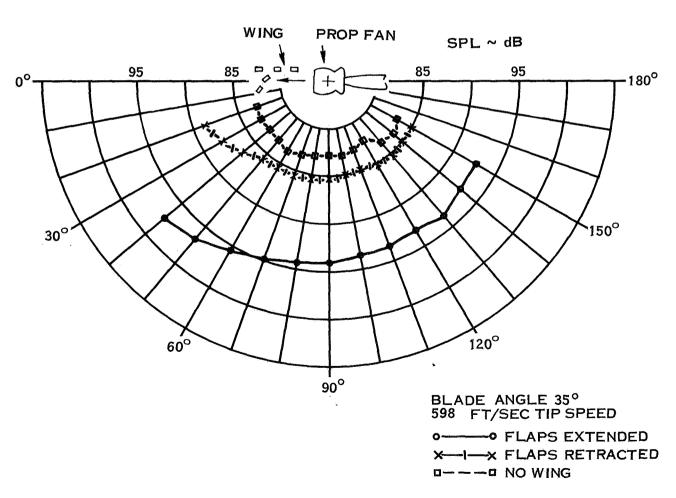
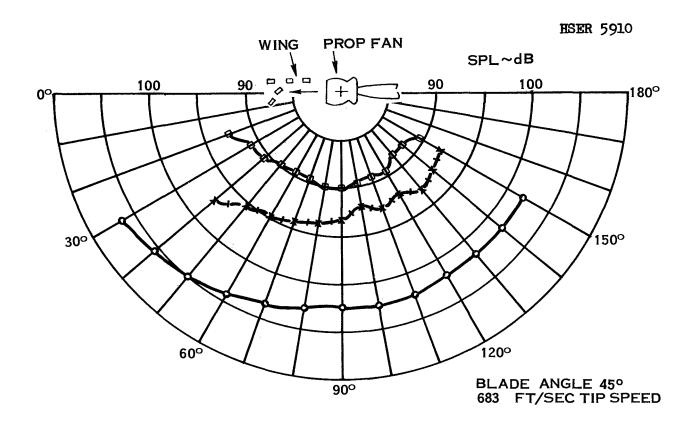


FIGURE 17 PROP-FAN STOL WING LOW FREQUENCY NOISE (112-449 HZ)



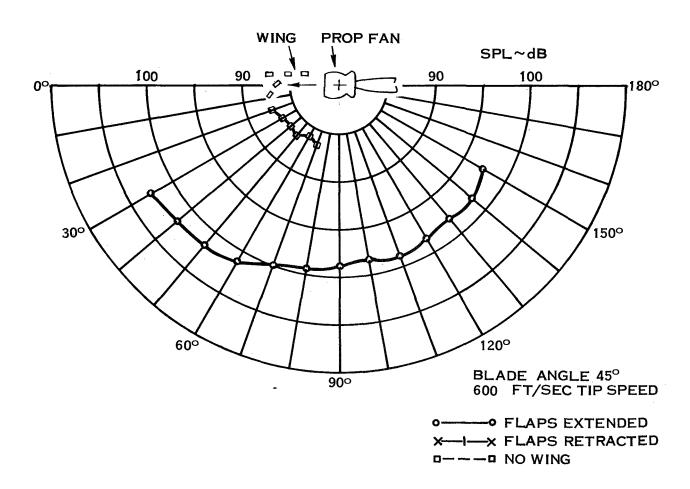
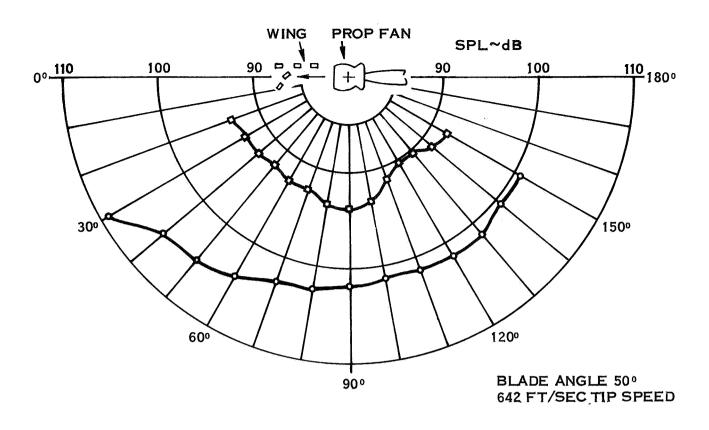


FIGURE 18 PROP-FAN STOL WING LOW FREQUENCY NOISE (112-449 HZ)



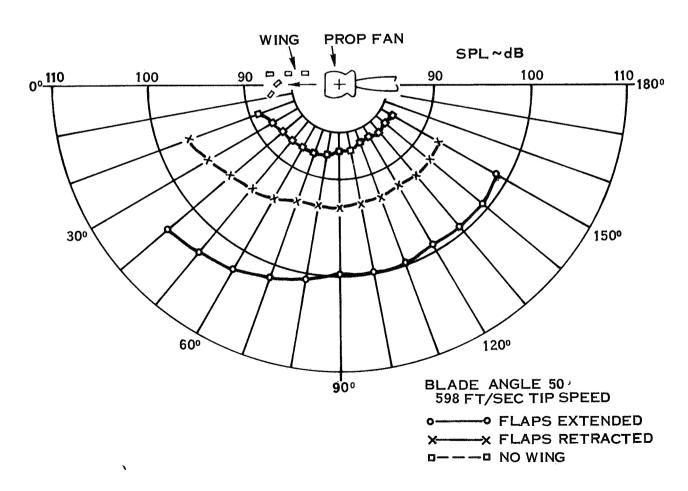
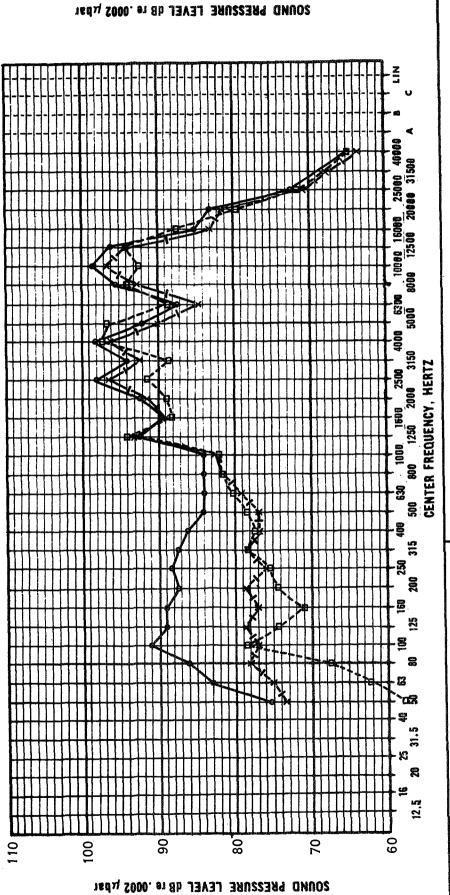


FIGURE 19 PROP-FAN STOL WING LOW FREQUENCY NOISE (112-449 HZ)



CENTER FREQUENCY, HERTZ	ONE THIRD OCTAVE BAND ANALYSIS O	NOISE X—I—X FLAPS RETRACTED  NO WING		No.
!	Hamilton U.Standard P.	TITLE PROP - FAN/STOL WING NOISE 35° BA 600 ft/SEC Vt	Test Date Run No. Mic Location $10^{1}-60^{\circ}$ Reel No.	Analysed By Identification No. Analysis Method Sheet

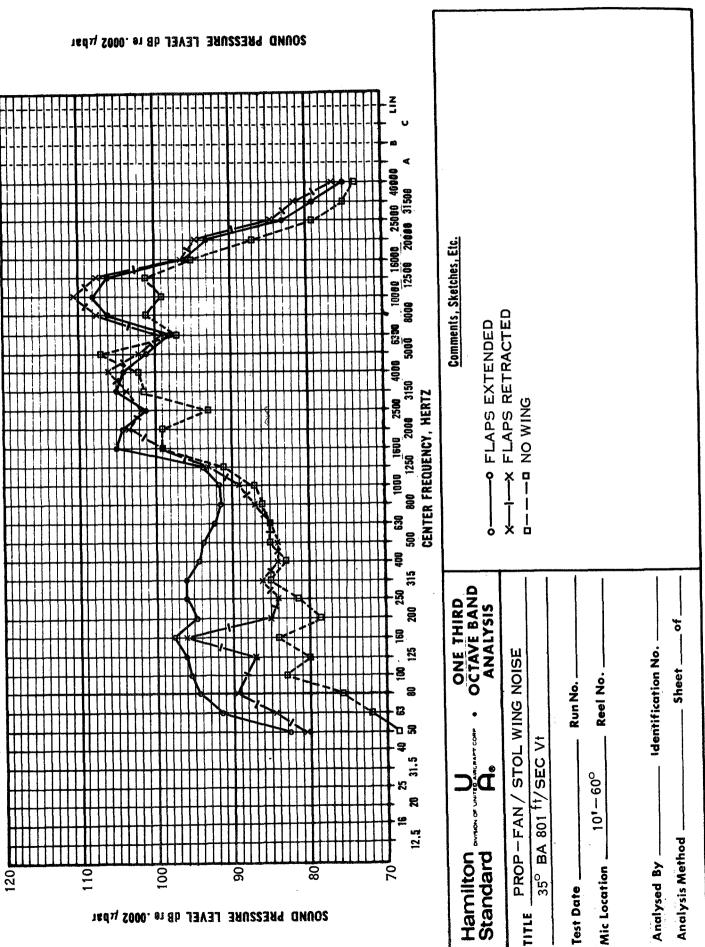


FIGURE 21

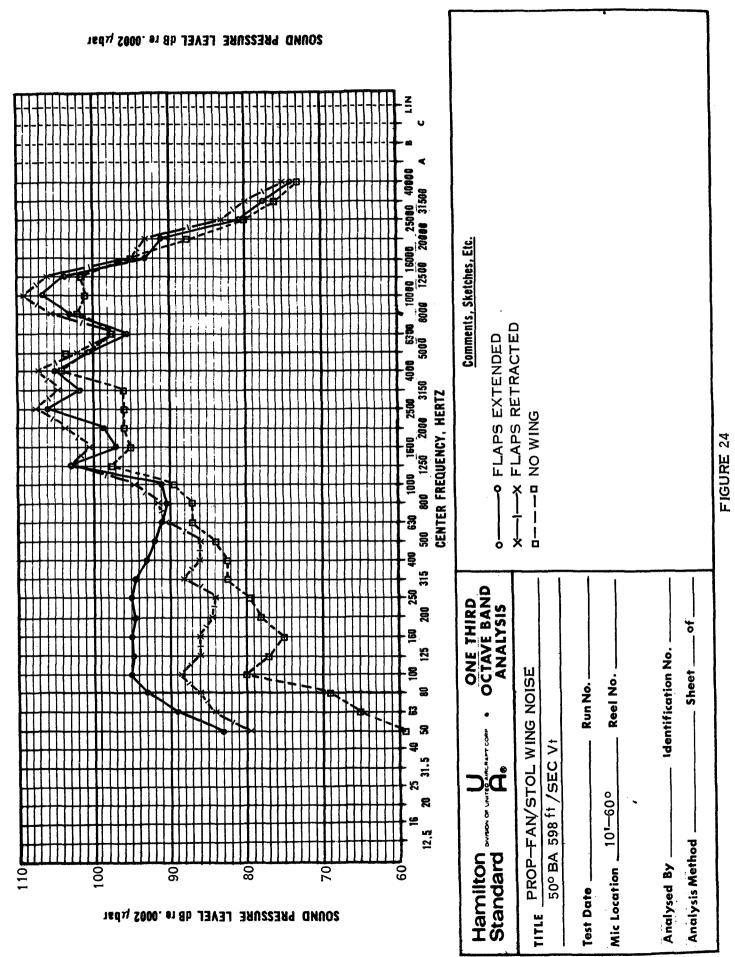
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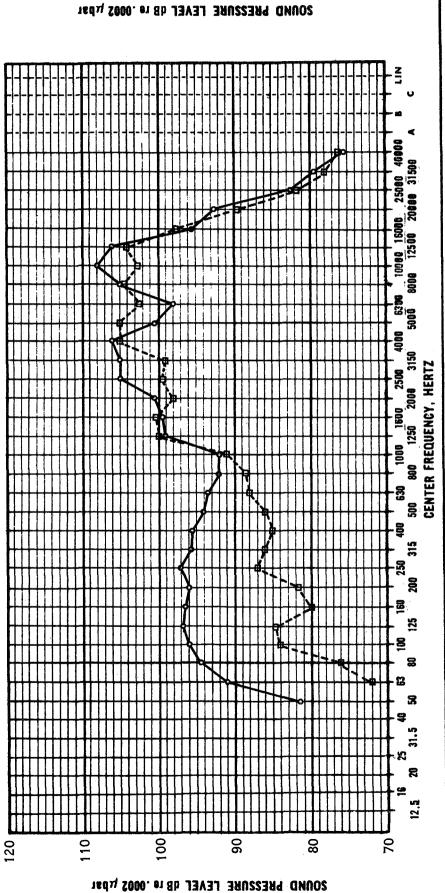
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SOUND PRESSURE LEVEL dB 18 .0002 pbst

GENIER PREGUENCI, MERIK	Comments, Sketches, Etc.	x x FLAPS RETRACTED		
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33



	VENIER FREGUENOI, MENIE
Hamilton Description OCTAVE BAND Standard As ANALYSIS	Comments, Sketches, Etc.
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Test Date Run No Mic Location 101 - 600 Reel No	
Analysed Ry	A.A.G.
po	7910

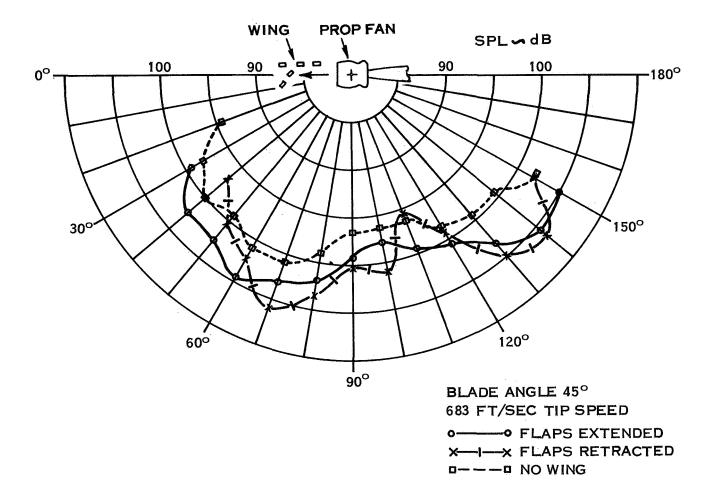
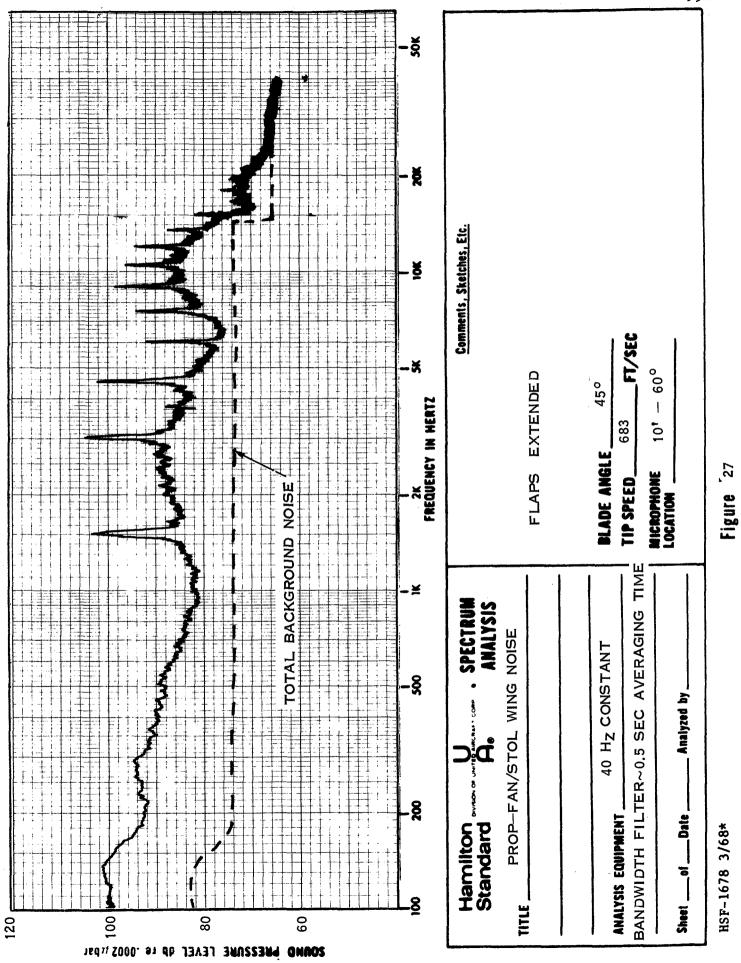
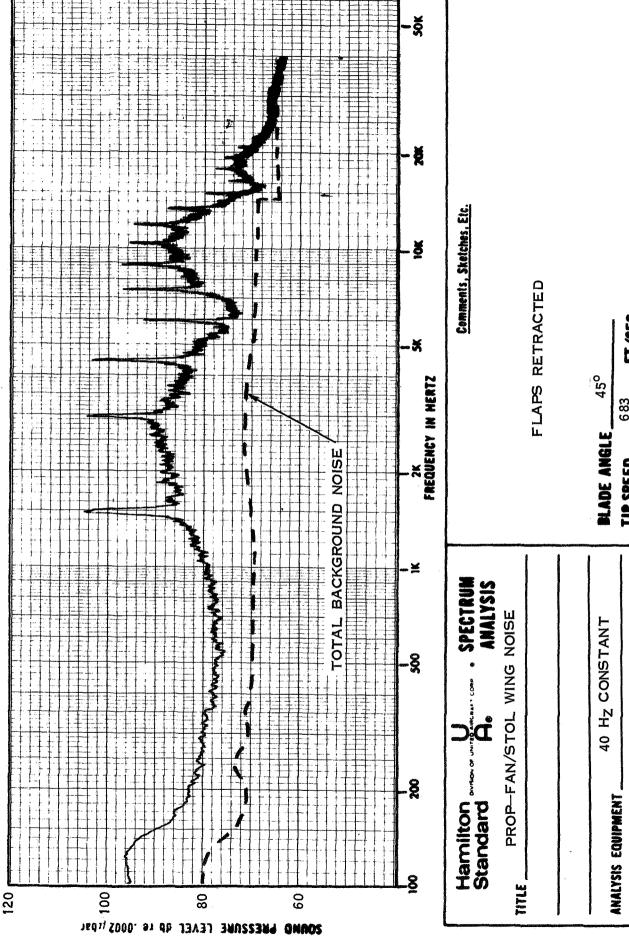


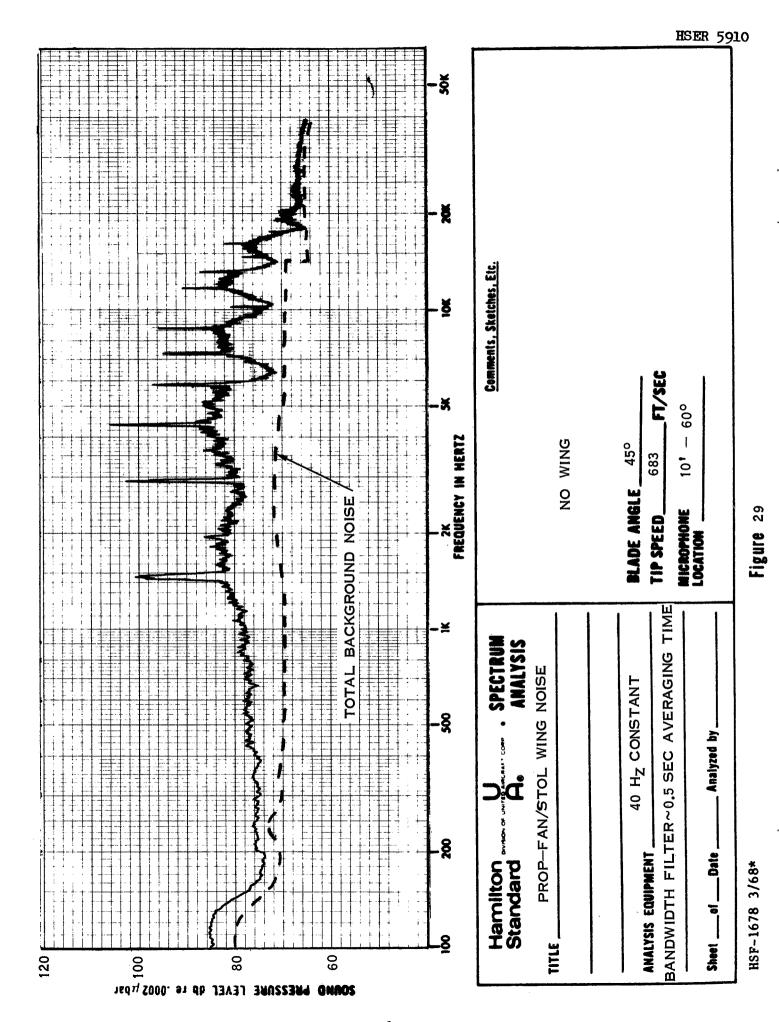
FIGURE 26 PROP—FAN /STOL WING NOISE FUNDAMENTAL OF BLADE PASSING FREQUENCY

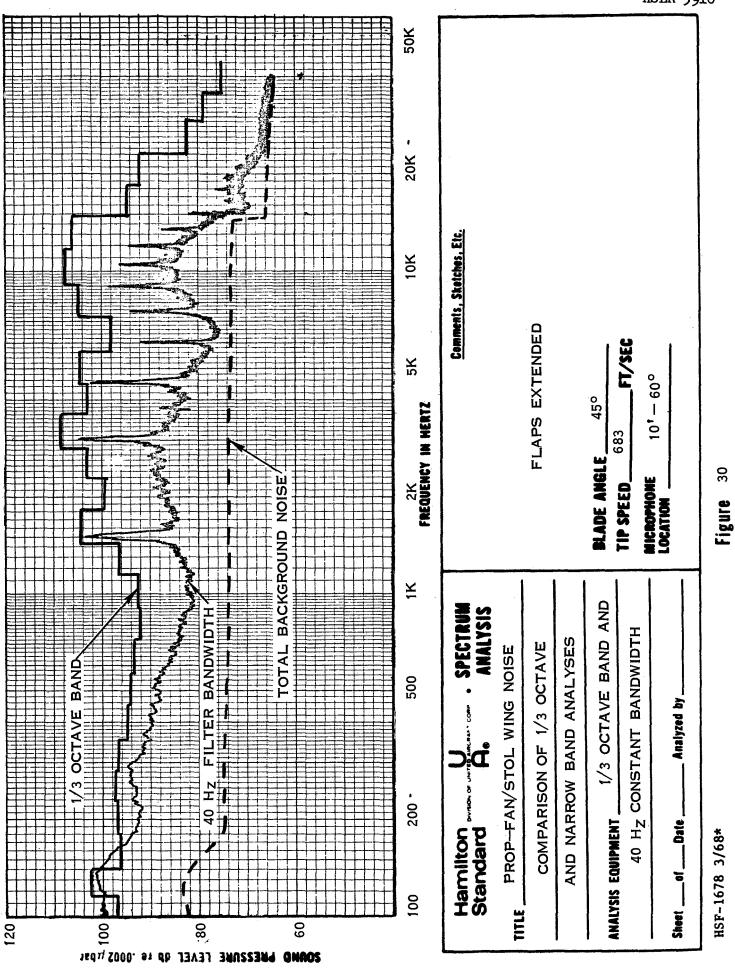


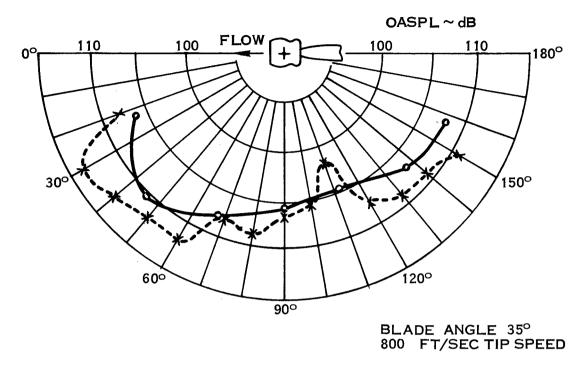
Sheet of Date

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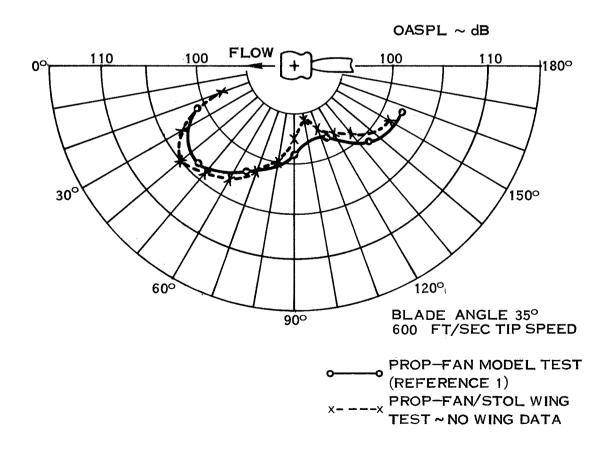
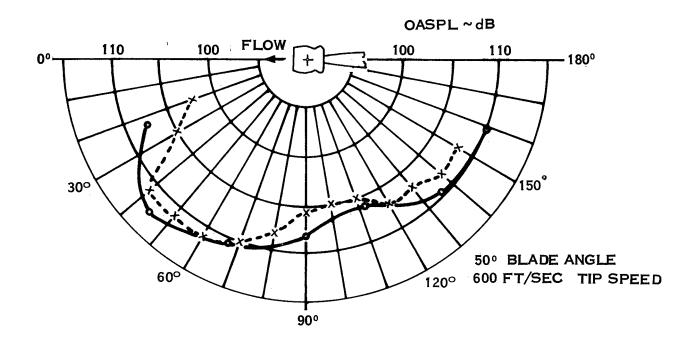


FIGURE 31. PROP-FAN NOISE COMPARISON CURVE



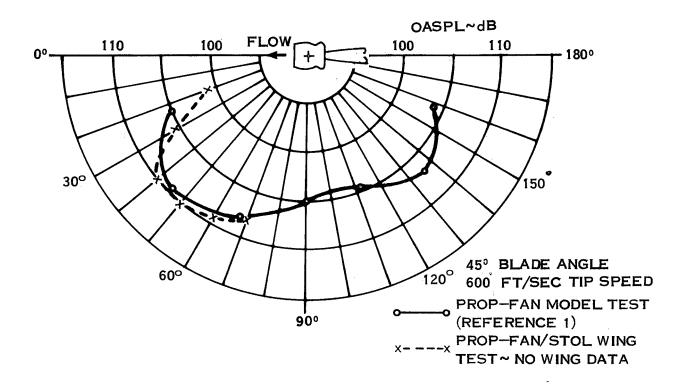


FIGURE 32. PROP-FAN NOISE COMPARISON CURVE

TABLE 1
PROP-FAN/STOL WING TEST CONDITIONS

Blade Angle (Deg)	Tip Speed (Ft/Sec)	STOL Wing Configuration
35 35 45 45 50 50	594 801 600 683 598 642	Flaps Extended
35 35 45	598 804 685 593	Flaps Retracted
50 35 35 45 45 50 50	593 600 801 598 683 599 641	No Wing

TABLE 2

PROP-FAN/STOL WING NOISE TEST

AMBIENT CONDITIONS

<u> Test</u>	Temp	Relative Humidity(%)	Barometric Pressure (In Hg)	Wind Velocity (KTS)
Flaps Extended	19 .	50	30.10	5-10
Flaps Retracted	19	50	30.10	5 <b>-</b> 7
No Wing	30	35	30.20	5

Hamilton U Standard AIRCRAFT CORPORATION A Re

#### APPENDIX A

ONE-THIRD OCTAVE BAND DATA



#### INTRODUCTION

This section contains the one-third octave band data for the sweep microphone, analyzed every 10° with a four second averaging time. The data is not continuous to zero degrees due to overloading of the microphone system caused by impingement of the Prop-Fan jet wake on the microphone. It should be noted that the data below 100 Hz is not considered completely reliable since this is the lower limit of the recording system frequency response (See Appendix B). In addition, data at frequencies above 15 KHz are influenced by total system background noise as shown in Figures 27 through 29. A detailed discussion of system and data accuracy is given in Appendix B.

TABLE 1A

### PROP-FAN MCDEL/STCL WING NCISE DATA

0

1 C ·

CONFIGURATION- FLAPS EXTENDED BLADE ANGLE-35.0
TIP SPEED-594.0

						A ZI MUTH		.E (DEG)	(9)				
0	140	130	120	110	100	ው	80		09	<u>ي</u> ر	04	30	20
~	68.	69	6	ċ	•	•	74.2	4	5	7.	7 •		
3	76.	76.	7	æ	ċ	•	-	3	3	'n	4.		
~	2.	82.	<b>m</b>	4.	• 9	•	-	9	• 9	•	7		
0	• 9	88	æ	<b>&amp;</b>	ċ	•	_	-	-	ံ	•		
2	86.2	88.0	87.5	88.2	88.0	88.5	0°68	89.2	89.0	90.2	0.06		
~	86.	87.	7.	<b>-</b>	<b>ф</b>		9	ထ	\$	ထ	6		
Q	87.	86.	5.	5	Š		9	• 9	<b>-</b>	6	•		
ι.	84.	83.	3	4.	4.	•	9	9	ъ Ф	6	0		
	83.	84.	4.	4.	4.	•	• 9	•	7	<b>6</b>	• Э		
	81.	82.	-	2.	3.		4.	5.	9	7	8		
U 1	80.	8C.	ċ	2.	3	•	4•	4	4	S.	9		
	79.	80.	-	-	-		3.	ŝ	4•	4.	ال •		
	81.	81.	1.	<u>-</u>		•	3	ω.	4.	4.	4.		
	82.	81.	င်	ဝံ	ċ		4.	3	4.	4.	5		
	• 96	92.		6	ċ	•	• 9	'n	4.	9	4.		
	87.	85.	4.	4.	4		6	$\infty$	ф Ф	6	<b>.</b>		
	89.	88.	•	5	5.	•	•		2	5	-		
•	.66 0	97.	•	Š.	4.	•	ထ	φ	ф Ф	φ.	• 		
	.06 2	89.	ဆိ	۲.	7	•	2.	2.	3	4.	5		
	. 46	93.	2	•	0	•	5	• 9	7	$\infty$	• Ф		
•	89.	88.	œ̈́	•	5		• 6	6	2.	'n	2.		
	83.	82.	-	ڻ	ं	•	*	5	7	<u>~</u>	•		
	93.	92.	-	ထံ	-	•	1.	3	5.	•	9.		
	·96 0	95.	4.	2.	ċ	•	<b>*</b>	•	• œ	ံ	•		
	. 46	92.	2.	ပံ	-			3	• 9	œ	œ		
	83.	82.	-	6	ф Ф	•	2	3	Š	<b>~</b>	э Э		
	81.	81.	<b>ب</b>	ထံ	4.		œ	6	3	4.	Š.		
	70.	•69	ထံ	•	4.	•	&	φ.	2	4.	5		
	68.	68	-	5	3	•	5	• 9	6		-		
	66.	65.	4•	8	2.	•	2.	2.	4.	• 9	•		
•	5 105.0	103.2	102.2	101.2	100.7	100.7	104.7	105.0	106.0	107.7	107.7		
•	6 115.0	114.8	115.0	115.2	115.0	115.2	118.5	118.4	118.5	118.4	117.7		

TABLE 2A

# PROP-FAN MCDEL/STCL WING NOISE DATA

0

CONFIGURATION- FLAPS EXTENDED BLADE ANGLE- 35.0
TIP SPEED-801.0

								A ZI MUTH	ANG	LE (DEG	(9)				
		150	140	130	120	110	100	Çr.	80	-	09	20	40	30	20
		~	-	œ	ဆီ	•	Ö		2	2	2.	'n	5.		
		S.	5.	•	-	<b>~</b>	ò		2.	ċ	-	2	2		
		0	ċ	ပံ	2.	2	50	•	5	4	4.	5.	9		
	O	4.	4	ŝ	9	•	\$	•	• 9	5	5.	Š	7.		
	2	2	4.	4.	S.	4	4	•	5	Š	•	<b>-</b>	<u>-</u>		
	9	-	-	8	6	ထံ	7	•	• 9	-	-	-	-		
	0	4.	4.	4.	3	4	4	•	4	4	4.	• 9	7		
	3	3	2	2.	2	ż	•		4	4.	• 9	7	8		
		2.	2	2.	2.	2.	~	•	4	4.	9	7	8		
u.	0	6	6	ئ	6	-	•	•	•	8	4.	5	• 9		
∝	Ċ	<b>-</b>	æ	ဆံ	æ	ငံ	•		2	2.	3	5	5.		
ш	3	-	8	ဆီ	æ	6	-		-	2	2	3	3		
c	0	<b>&amp;</b>	<b>&amp;</b>	8	7.	ထံ	6	•	0	-		-	2		
	00	8	ф Ф	8	œ	~	œ	•	. 6	0	-	\$	2.		
	25	ċ	• 6	0	6	ထီ	8	•	-	2.	3	3	3		
z	009	103.7	103.5	105.0	102.2	97.7	98.2	98.5	100.2	0	105.0	103.0	102.0		
	00	2.	•	4.		-	8	•	00	02.	04.	5	02.		
	50	• 96	95.	95.	95.	4.	5	•	0	01.	01.	٠ د	01.		
'n	15	03.	•	-	-	Ġ.	•	•	03.	04.	05.	• 9	05.		
	00	•	6	00	ထံ	<b>.</b>		•	!	2	4.	4	03.		
5 2	00	. 66	<b>'</b>		<b>.</b> -	4.	Š	•	6	01.	01.	-	01.		
9	30	5.	3.	4.	<b>.</b>	2	-	٠	9	96	<b>&amp;</b>	6	6		
œ	00	02.	01.	01.	01.	6	å	90	03.	ŝ	90	5.	90		
	00	9	5.	'n	5	÷	2	•	5.	90	<u>-</u>	6	·		
	50	03.	(3.	03.	02.	ပ္ပံ	00	01.	03	04.	05.	7.	08.		
	00	3,	3	3	3		ċ	•	6	<b>,</b>	Š	7	œ		
20	00	2.	2.	2	2.	ဝံ	<b>œ</b>		6	ċ	<i>ب</i>	4	5		
	00	-	-	•	-	6	7	•	•		ċ	4	S.		
	50	6	0	6	6	ထံ	9	•	• 9	8	6		2.		
	00	9	7.	• 9	7.	5.	e.	•	2	3	4.	•	7.		
$\Box$	7	113.2	112.5	112.5	112.0	109.5	109.7	1111.0	113.0	113.7	115.2	115.2	116.0		
PNL 1	0 F.I V E.R	119.3	120.4	122.4	122.8	121.8	122.3	123.7	125.6	126.2	126.7	126.2	124.1		

TABLE 3A

# PROP-FAN MODEL/STOL WING NOISE DATA

0

10

(DEG)

AZI MUTH ANGLE

CONFIGURATION- FLAPS EXTENDED BLADE ANGLE- 45.0
TIP SPEED-600.0

	150	140	130	120	110	100	06	80	10	99	20	40	30	20
	0 74.	75.	•	7	-	7.		6	0		-	4.	• •	
•	3 81.	82.	4.	3	*	4.	•	7	8	ф ф	8	9	6	
	0 87.	88.	8	ထိ	<b>5</b>	6		2	2.	-	2	2.	8	
1(	0 91.	93.	2	2.	3	3	٠	5	5.	Š	4	4.	-	
ri	5 89.	.06	ö	-	3	. • 	•	3	8	4.	4.	4.	• 9	
1(	0.06 09	91.7	91.2	93.0	92.7	93.0	7.66	93.0	95.5	93.7	94.2	95.0	95.2	
5(	0 92.	92.	-	-		ö	•	-	2	3.	4.	4.	4.	
2	.06 0	89.	6	6	ငံ	6	•		2	4	3	5	Š	
m ·	5 89.	• 06	ပ	ပံ	ċ	ċ		•	2.	69	4	4.	5	
4	0 86.	87.	7	•	7	8	•	6	ċ		8	3	3.	
N	c 85.	86.	Ŋ.	•	<b>&amp;</b>	7.	•	6	6	0	-	2.		
•	0 85.	85.	5	7	•	-	٠	&	6	•	ċ	ċ	ċ	
8	0 86.	86.	5.	9	•	• 9	•	œ	• Ф	6	6	6	<b>&amp;</b>	
10	0 88.	87.	•	5	•	•	•	7	œ	6	0	•	8	
E 12	0 100.	66		7		3	•	œ	4.	Ö	•	ċ	5.	
16	0 92.	91.	°	ö	ċ	6		2.	ζ.	4.	4.	4•	_	
20	0 93.	93.	2	å	2	2.	•	• 9	•	-	œ	<b>-</b>	÷	
25	0 105.	104.	3	2	_;	ċ	•	°.	3.	05.	90	08.	4.	
	0 97.	97.	•	5	ů	5.	•	æ	6	Ö	2.	3	œ	
40	0 100.	102.	2.			<b>&amp;</b>	•	33	4.	05.	90	90	ċ	
$\circ$	. 66 0	686	œ	œ		7	•	6	03.	04.	05.	04.	00	
(1)	0 95.	95.	'n	4.	3	2.	•	3	•	œ	6	6	• 9	
0	.06 0	89.	ċ	6	φ,	8	•	-	-	m •	4.	5	3	
00	. 86 0	98	7.	~	•	4.	•	7	<u>-</u>	•	2.	2 •	-	
25	0 102.	102.	2.	-	ပံ	-		-	-	•	• 9	• 9	ċ	
0	c 97.	97.	7.	•	ŝ	2.		5	9	œ	·	ċ	<b>†</b>	
00	0 84.	85.	4.	3	2	ċ		3	4•	• 9	7	œ	3	
50	0 82.	82.	-	ؠ	6	• 9	•	• 9	•	6	ċ	-	•	
15	0 77.	77.	•	Š	<b>.</b>	2.	•	33	4	9	9	7	4	
00	0 75.	75.	5	4.	3.	•	•	-	-	2	3	6	<del>.</del>	
D 8 (1		110.0	109.5	109.2	108.5	107.5	108.7	110.5	1111.2	113.0	114.0	114.5	1111.2	
PNL 10F	-													
Λ0		120.2	120.9	121.2	121.8	121.2	122.4	124.5	124.7	125.3	125.4	124.2	118.8	

112.9 112.5 112.5 110.5 111.0 110.2 110.5 114.0 114.2 115.5 116.2 116.2 113.5

121.8 122.1 123.9 122.4 123.7 124.1 124.2 128.4 128.1 128.4 127.4 125.0 121.4

DB(L) PNL 10FT FLYOVER

ABLE 4A

PROP-FAN MCDEL/STCL WING NOISE DATA

0

10

(DEC)

AZI MUTH ANGLE

CONFIGURATION- FLAPS EXTENDED BLADE ANGLE- 45.0 TIP SPEED-683.0

20																															
30	6	04.	4.	01.	03.	6	8	6	8	•	5.	3	-	-	8	6	4.	ф Ф	105.7	6	•	7	ċ	0.2.	6	2.	Š	ф ф	ŝ	4	
40	5	8	4.	8	4	-	8	6	8	<u></u>	9	4.	2.	3	•	3	8	02.	108.7	03.	03.	œ	5.	6	-	9	4.	4.	•	٠. و٠	
20	2	-	4.	•	2	-	7	æ	<b>α</b>	ô.	5	4.	3	~	•	2	6	w.	108.5	6	6	6	•	6	7.	9	4.	3	0	\$	
ე9	2.	<u>.</u>	Š	• 9	2.	• 9	•	-	.9	4.	4.	3	2	2	• 9	4.	• 6	03.	108.5	03.	04.	98	05.	7.	90	4.	2.	2	6	rU •	
70	2.	<del>-</del>	4.	• 9	-	9	5	9	5	4.	3	9	2.	-	9	33	ф Ф	02.	108.0	01.	00	٠.	2.	• 9	33	3.	• 6	•	•	3	
80	2	5	<i>ن</i>	9	_	9	4.	Š	4.	ښ •	3	2	2	0	4	2.	ф Ф	02.	108.0	02.	02.	4.	2	05.	02.		<b>ф</b>	ф Ф	ŝ	3.	
06	•	•	•			•			•	•						•			101.7	•	•	•	•	•	•						
100	9.	8	3	9	9	7.	3	4•	3	2	2.	2.	ċ	6	-	<b>ф</b>	ŝ	7	102.5	7	• 9	2.	6	2.	6	φ.	7.	7	• 9	5.	
110	6	<b>*</b>	2	•	•	•	5.	3.	3	2.	2	ċ	ပံ	6	2	6	4.	•	102.5	•9	•	2	တံ	å	ပံ	ဝံ	Ġ,	6	6	~	
120	8	5	-	5	8	Š	Š.	8	3.	-	•6	ċ	6	6	5.	ċ	4.	9	101.2	<b>.</b>	•	2.	00	4.	00	•	2,	•	္ငံ	œ	
130	œ̈́	ທໍ		5	o,	ς,	Š	ů	<del>"</del>	•	\$	÷	÷	6	4.	3	5.	æ	105.2	.66	6	3		05.	02.	2.	2	<u>,</u>	• i	6	
140	•	-	-	5	œ	5	4•	3	<del>.</del>	2.	6	<b>œ</b>	• 6	0	9	5	.96	æ		0	01.	2.	•	0.5	05.	2	<b>~</b>	• ,i	-	6	
150	<b>&amp;</b>	•	6	4.	4.	4.	5	'n	2	<b>?</b>	6	<b>ф</b>	6	0	• 9	5.	•	.00	108.1	98.	œ	<b>~</b>	• 	4.	2.	\$	2.	_	-	œ	
	50			0	$\sim$	9	0	S		40	0	63	80	100	125	160	200	250		00	200	30	800	000	50	009	000	500	150	000	

117.4 120.9 121.3 122.2 121.3 123.0 123.8 125.0 126.4 125.9 124.6 123.1

PNL 10FT FLYOVER

TABLE 5A

# PROP-FAN MCDEL/STCL WING NOISE DATA

0

10

20

CONFIGURATION- FLAPS EXTENDED BLADE ANGLE- 50.0 TIP SPEED-598.0

							AZIMU	H ANG	030) 31	(5)			
	150	140	130	120	110	100	06	80	10	ე9	20	40	30
50	5.	9		7.	8	80	0	2	2	3	'n	4.	
63	82.5	83.5	84.0	84.7	85.7	86.2	87.2	88.7	89.2	89.2	89.7	0.06	
80	-	8	0,	ံ	ပံ			2.	3	3	4.	3	
$\circ$	2.	4	3	3	4	•	5	ريّ •	•	'n	5.	•	
$\sim$	-	<b>!</b>	3	3	6	4	3	4	5	4	Š	5	
Ç	•	3	2.	3	4.	3	3	4	4.	5	5.	5	
0	3	3	2	2	2.	2.	2	2	8	4.	5.	•	
S		•	0	ċ	-	•	2.	2.	3	ις.	ις.	• 9	
~	0		-	2.		ċ	-	2.	3	4.	U.	. 9	
40	œ	8	œ	<b>&amp;</b>	æ	6	•			60	4.	5	
50	•	•	•	-	Ö,	6	ċ	2			w.	4	
63	•	~	-	ф ф	œ	6	ċ	• l	0		2.	2.	
80	-	œ	<b>ب</b>	7	7	8	œ	•	0	0	0	0	
0	6	. 6	œ	-		-	8	6	ò		Ξ.	<u>-</u>	
125	<del>ا</del>	2	φ,	œ	Š.	8	•	7	2	60	8	ф Ф	
160	3	• 46	2.	2	-	2	2.	4.	•	. 96	5	v.	
200	5.	• 9	5.	5	<b>.</b>	ıÇ.	•	8	6	œ	6	8	
250	6	4	8	2.	ô	2	3,	3	0.6	05.	05.	05.	
315	-	98		<b>~</b>	5	• 9	7	6		01.	02.	04.	
H 4000	80	•	5			8	0	3.	05.	Š	4.	3	
200	S	•	Š.	ŝ	<b>*</b>	4	5	<u>~</u>	6	00	.00	01.	
30	•		•	ô	6	6		~	3	3	5	96	
00	00	00	000	φ,	å	7	-	00	01.	03.	8	03.	
000	03.	•	3,	03.	-	ċ	•	Ψ.	4.	9	8	-	
250	•	0.2.	01.		6	8	00	00	02.	03.	ۍ.	05.	
00	•	٥,	2		<b>6</b>	8	8	6	,i	3	S.	4	
000	2.	<u>٠</u>		-	<b>&amp;</b>	<b>-</b>	9	7.	-	-	2	2.	
500		•	ပံ	6	2	•	•	-	φ Φ	ċ	-	2	
150	0	•	္ပံ	6		5	4	5	ហ	<u>/</u>	8	• 6	
000	œ	• 63	-	•	5.	m	÷	2	2	3.	4	4.	
08(L)	110.2	1111.5	109.7	110.2	108.5	109.0	109.5	1111.0	112.7	113.7	113.5	114.0	
(													

113.0 113.5 112.5 111.2 110.2 110.5 111.5 113.7 114.0 115.0 115.5 116.5 115.5

119.6 122.1 122.7 123.0 122.6 123.5 125.2 127.0 126.7 127.0 126.8 125.5 120.6

PNL 10FT FLYDVER

DB (1, )

TABLE 6A

### PROP-FAN MODEL/STOL WING NOISE DATA

0

10

20

CONFIGURATION- FLAPS EXTENDED BLADE ANGLE- 50.0 TIP SPEED-642.0

	30	0.4.	08	08	07.	ŝ	02.	6	8	ထ	÷	\$	2	ô	ô	Š	<b>*</b>	<b>*</b>	02.	3	00	\$	Š	7.86	ô	8	ငံ	<b>4</b>	-	4.	3	
	40	Š	2	4	•	œ	7	œ	œ	œ	<b>-</b>	9	4.	ò	Š	01.		• 66	90	07.	5	01.	• 66	106.0	60	07.	-	. 4	4	ó	• 9	
	20	S	2	4	-	<b>,</b>	-	9	œ	7	9	Š.	4.	W	ις: •	œ	Ġ	01.	90	07.	9	00	6	105.2	Ġ.	<b>!</b>	ŷ	ŝ	e,	ċ	ė	
_	09	6	ە. بىب	4	Š	9	9	9	<u>.</u> جر	5	Ŋ	4.	ις •	à	å	6	6	0.0	05.	05.	ş	00	œ	105.0	0.8	06.	5	2	2	6	ιυ •	
LE (DEG	70	2	6	ξ.	•	•	9	4 •	'n	4	3,	3	33	7		6	ę.	9	05.	4.	03.	6	9	104.7	90	0.4	3	0	0	•	4	
ANG	80	. <b>0</b> .pm4	ċ	4	9	50	5	<b>*</b>	4.	4	2	2	2	ه نسر	0	8	<u>.</u>	6	05.	5	03.	<u>.</u>	5.	104.0	05.	03.	2.	6	6	9	6	
A ZI MUTH	06	•			•		•	•	•		•		•	•	٠			•	05.		05.			100.2	03.	•					•	
	100	0	œ	5	•	4	5	3	4	2.	*	2.	2	0	Ġ	Š	9	• 9	00	ċ	00	Š	2	66.5	02.	ô	6	œ	œ	7	4.	
	110	8	ထီ	8	•9	Š	5	*	3	2		-	ငံ	6	6	*	4	5	6	6	ô	ķ	ผู	100.0	\$	00.	ပံ	ô	6	œ	9	
	120	Ď,	•	2	'n	ķ	ķ	<b>*</b>	å	6	ပံ	ċ	ô	6	6	8	œ	Š	01.	01.	ô	95.	93.	101.C	04.	02.	92.	2	-	ငံ	å	
	130	4	•9	ਹੰ	ķ	ιυ,	'n	4.	2.	2.	ċ	6	ငံ	6	o	0 0	ċ	96	02.	2	02.	9	œ.	101.5	05	02.	ς.	چ	2	-	ထို	
	140	7	9	ċ	4.	4.	4	3	2	?	٠ •	œ	6	6		¢3.	3	97.	03.	•	02.	• 9	ري ه	101.5	05.	03.	3	2	2	82	6	
	150	Š	8	0	8	8	m	4	8	2 .	6	œ	œ	c.	ိ	6	· α	• 9	04.	03.	•	• 96	4	102.2	.90	4.	, t	4	3	60	Ċ	
					0	N	9	0	5	فسيسور	40	0	63	80	100	125	160	200	250	15	400	00	30	8000	000	50	009	000	50 C	150	000	

PNL 10FT FLYOVER 111.2 112.3 112.6 112.3 111.4 111.9 112.9 114.7 115.8 116.4 116.0 115.8 111.3 108.8

TABLE 7A

# PROP-FAN MCDEL/STCL WING NOISE DATA

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CONFIGURATION- FLAPS RETRACTED
BLADE AVGLE- 35.0
TIP SPEED-598.0

	20	7	6	6	6	7	2.		79.7	ċ	-	6	è.	ċ	ċ	œ	• (-	'n	•	œ	2.	ф Ф	4	œ		œ	ċ	5	• 9	ů	÷	100.7
	30	2.	•	8	6	<b>;</b>	_;	•	19.0	ċ	7	æ	<b>&amp;</b>	•	2	3	•	7.	<b>-</b>	-	5	6	• 9	3	<b>-</b>	3	2.	6	6	•	ကို	103.5
	40		5	<b>-</b>	<b>α</b>	•	•	• 6	78.5	8	7	7.	6	-	3	5.	7	•	•	4	7.		5.	5	• Ф		9	3	3	•	5.	106.0
	20	2.	ŝ	-	ъ Ф	6	7.	6	77.5	8	• 9	-	œ	_	å	4	7	-	œ	2.	•	0	9	3.	<b>ф</b> .	•	5	2	2	6	4.	105.2
	<b>09</b>	3	ۍ ک	œ	-	о Ф	-	œ	76.0	œ	• 9	• 9	6	-	2.	3	· α	-	•	2	-	0	4•	2.	•	4	ω -•	-	-	œ	3	104.0
0	~	2.	3	7.	-	6	Š	6	7.97	œ	9	• 9	ထ	-	_	-	7	Ö	9	2	4•	œ	<u>.</u>		4	-	ċ	ъ Ф	7	4•	۲.	102.5
ANG	80	6	3	<b>'</b>	4•	0	9	9	76.5	-	6.	9	• Ф	0	0	6	9	6	4•	•	3	7	-	0	2	o	6	9	\$	3.	•	101.0
A ZI MUTH	6	• 9	2.	• 9	5	2.	• 9	4.	75.0	6	4.	4.	7	8	œ	œ	3.	9	3	-	6	4•	• 6	• 9	• 6	9	5.	3	3.	-	6	98.7
	100	7.	-	5	4.	-	5.	5	74.2	6	4.	4.	• 9	œ	8	ф Ф	3.	5.	2.	3	œ	33	<b>&amp;</b>	'n	8	5	5.	2.	2.		ċ	7.16
	110	4.	ဝံ	'n	2.	ပံ	5		75.0		3.	ທໍ	9	-	8	<b>!</b>	3	ŝ	-	•9	6	m	6	•	6	<b>.</b>	-	5.	4.	3,	<b>.</b>	98.2
	120	3.	6	4	8	°	9	9	74.5	8	4.	5	7	8	ထံ		4.	•	å	<b>-</b>	ö	4.	6	œ	2.	ံ	6	ထိ	9	5.	4.	7.56
	130	4	œ	W.	ъ.	ပံ	•	-	75.0	6	4.	5	-	8	5	-	Ŋ	-	5	ထံ	2.	5	ċ	6	ć,	ပံ	0	Ġ.	7	•9	4.	101.5
	140	2	•	-	4.	0	5	7.	75.2	-	4.	5.	7	6	6	3,	• 9	7.	7.	<b>∞</b>	2.	9		0	4.	-	-	•	œ	7	5.	102.2
	150	2.	S	ċ	-	œ	5	•	7.97	-	5.	9	-	•		9	9	φ Φ	8	0	2.	•	2.	2.	5	5	~	<u>;</u>	6	<b>œ</b>	5.	103.5
									250		40	50	63	80	100	125	160	00	250		400	00	30	00	000	250	00	000	500	150	000	08(1)

117.7 120.4 120.3 119.9 120.4 122.1 122.9 123.8 125.9 126.2 124.7 122.9 119.2 115.2

FL YOV ER PNL 10FT

TABLE 8A

## PROP-FAN MCDEL/STOL WING NOISE DATA

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(DEG)

AZIMUTH ANGLE

CONFIGURATION- FLAPS RETRACTED BLADE ANGLE-35.0 TIP SPEED-8C4.0

140	130	120	Ç	100	000	200	.t 10t	09	50	04	30	20	10
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	4.	5.	-	7.		<b>~</b>	6	6	6	0	•		
	9	8	œ	6		6	6	œ	6	6	0	2	
	7	6	ပံ	6		•	9	7	ထ	6	0	8	
	5	6	ပံ	0		œ	œ	Š	4.	3	4	3	
	3	8	6	2.		33.	4.	5	5	• 9	-	æ	
	2.	•	_;	-	•	6	4.	3	4.	5	-	00	
	87.2	85.7	85.5	85.0	86.2	86.0	87.7	86.2	87.0	87.0	88.2	89.2	
	2.	•	2.	2.	•	3	ä	4.	ŗ,	5	Š	• 9	
	2.	2.	2.	-	•	3	3	3	4.	4.	5.	•	
	4.	3	÷	8	•	3.	5	5	5	S	5	5	
	4.	4.	4.	5		Š	•	/	7	~	• 9	œ	
	•9	5.	5.	5		•	ф Ф	6	ं	0	8	8	
	<b>&amp;</b>	æ	-	8		-	2.	3	2	<b>?</b>	ċ	<b>&amp;</b>	
	ထီ	•	-	5.		9	6	9	œ	6	6	• 9	
_	2	6	ငံ	6	•	•	03.	03.	01.	3.	2.	6	
	95.	4.	4.	5.		00	-		ċ	0	• 9	5	
	<b>&amp;</b>	<b>!</b>	<b>.</b>	œ		-	03.	04.	04.	3	<b>-</b>	-	
-	ပံ	æ	œ	ċ	•	02.	05.	• 90	90	4.	03.	03.	
	4.	4.	4.	۲.	•	<b>-</b>	6	C1.	00	3	00	7	
	2.	2.	2.	2	•	4•	۲.	6	98.	<b>ө</b>	• 9	Š	
,	01.	00	6	6	8	2	04.	. 20	05.	-	03.	•	
•	5	4.5	03.	2.		•	œ	ò	ċ		•	2	
	02.	02.5	ငံ	ċ	01.	3	05.	. 10	07.	æ	02.	9	
	3,	4.	-	ċ	•	2	4.	9	8	6	å	2	
	3	3	ċ	œ		•		4.	'n	7.	ċ	4.	
		-	6	8		0	2	4.	'n	9		8	
	ċ	ċ	-	9		7	œ		2	3	<b>&amp;</b>	S.	
	٦.	7.	9	4.	•	8	4.	9	7	8	4•	60	
•	1111.C	110.2	109.2	109.5	110.5	112.0	114.0	115.5	115.2	116.2	112.5	110.5	

118.9 121.6 123.4 120.5 121.2 122.3 127.3 127.1 129.4 127.8 126.1 121.4

DB(L) PNL 10FT FLYOVER

TABLE 9A

## PROP-FAN MCDEL/STCL WING NOISE DATA

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M O	9	- FL	APS RET	TRAC TED	•								
TIPS	PEED-	•											
							A ZI MUTH	4 ANGLE		_ '	Ç	<b>C Y</b>	30
	150	140	130	120	011	100	06	œ	10	9	ň	}	3
				1	1	,	0	79.	8	83.0	83		
50	71.	76.	74.	-	ά,	•	0 0	70	20.	86.5	86	87.	
63	76.	79.	81.	81.	8 I.	91.	0.0	0	0 00	89.5	90	91.	
90	80.	83	85	82	8	800	•	0	0	89.2	89	95.	
100	85.	86.	88	87.	ထီ တ	200	0 0	0 0		7.96	96	96	
125	91.	95	95.	88	ထိ	94.		0.0	7	88.7	89	91.	
160	84.	86.	86.	86.	86	8	8 8	0 u	9	86.2	86	88	
200	833	84	84.	83.	83	8	82	620	ם סנק	84.7	8 6	87	
750	85	84	84	82.	83	82	82	000	) is	7.58	86	87	
315	82	83	83	83	83	82	× ×	÷ .	0 a	25.7	80	86	
1 4	94	28	85	83.	83	82	32	, t	0 0	. v	00.00	86	
· u		83	82	82	81.	8	8	20 0	0 0	י ער כי מי	ς γ (ς	86	
٠ <u>٠</u>	, w	86.	84	84	85	84	84	200	0 0	, c	α α	87	
ò	2 0	86	86,	85	86	84	8	\$ 6	<del>-</del> c	000	0 0	6	
, ,	- α	00	8	86	86,	85	8	8 9	2 6	0 4 4 0	0 0	6	
2 6	מ	96	94	06	8	92	92	66,		1001	, 0	16	
77	101	106	104	66	95	101	100	103	0 0	200	, α ) σ	95	
200	96	96	95	46	95	95	98	66	100	7000	, ,	6	
ט ע	200	000	97	96	9.7	97	101	103	001	2001	2 0	105	
22	104	104	105	100	100	101	107.5	106.7	110.2	20.601	100.0	00	
10	00	0	66	96	97	4	103	102	104	100		0.7	
· ·	00	2	100	95	96	95	104	101	<b>1</b> 04	1000	2 0	, ¢	
200	70	93	95	93	91	91	95	96	7	10.40	10	100	
00	101	100	101	66	86	98	101	103	001	1100	2 5	103	
	104	10.0	105	102	101	101	104	109	707	108.0	2 0	101	
א כיי	103	103	102	100	66	66	53	* O T	2 0	0.40	0	92	
) (	200	70	6	96	8	8.7	91	5	) (		Ö	ά	
9 6	0 0	6	6	8	80	86	8	90	2,	4.0		2 6	
	, c	. 0	ά α	7.0	3	76	19	8	8	x + .	0	- 1	
20	n (	0 0	0 0	. 7	~	76	7	78	8	81.4	o i	- 1	
31500	83.7	, x	80.2	77.2	76.2	73.2	14	74	16	77.5	_		
	É	G	Ś	•					,	,	4	110.2	
DB (1	1111.2	113.0	112.5	108.7	108.7	109.	0 113.5	114.0	116.5	0.011	•	2	
1001 INC	1						1		2001	127.8	126.1	121.4	

TABLE 10A PROP-FAN MCDEL/STCL WING NOISE DATA

(DEG) CONFIGURATION- FLAPS RETRACTED BLADE ANGLE- 50.0 TIP SPEED-593.0

10															_			_	~	10	^			. c		<b>7</b> U	O F	- (	1 C	- (	0	0	£0		0		9		
20	82.5	87.	89.	91	06			œ œ	87	88	8.7	88	α	0		0 0	9	9	96	101	100	201	6	6	,	, (	, i	,	,	x	-	_	7		109.	ŀ	113.		
30	7.67	85.0	88.7	7.08	, oa	7.00	0.48	87.0	86.5	87.5	87.5	87.2		010	7 1 0	92.2	99.5	0.96	98.7	105.7	102.0			000		1001	103.	101	91.	88	80.	78.	75.		112.0		119.9	4	
40	79.	84.	86.		,	200	87	85	84	7	9 0	- a	0 0	000	7	93	100	97	102	101		27	2	2	6	106	109.5	0	6	6	œ	α	, ,	-		011	124.7	- 71	
50	80.	3		- (	200	8 7	86.	8 4	4	0	0 0	1 0	Ω	8	92	94	100	100	2 6		2 :	901	0	10	6	2	109.5	2	6	6	α	a	1 0	_		1.10.0	,	071	
ر 90	7.07			20.0	88.5	86.2	86.2	84.5	100	000	200	86.2	86.2	90.5	91.5	94.5	7.001	100		103.0	C . J CT	104.5	107.0	102.0	97.5	105.5	109.2	106.0	94.7	03.6	0			1.2	1	115.0	ľ	7.121	
(DEG) 70	70	7.0	81.7	86.5	88.0	85.0	0.58		000	80.00	87.5	85.7	85.5	89.2	91.2	92.5	7 101	101	7.001	103.2	107.5	103.5	107.2	101.5	95.0	103.2	107.0	104.5	92.7	7		2.18	0.87	74.2		114.2		127.5	
ANGLE 80	ì	0.0	81.5	86.7	7.68	86.0	2 2 2	7.00	6.78	84.0	86.5	84.7	84.2	87.7	89.5	000	76.6	66.5	6.86	102.2	105.0	102.2	103.5	99.2	93.7	102.0	105.2	103.2	1 10		34.0	C 61	77.0	73.2		112.2		125.5	
ZI MUTH 90		16.1	80.7	85.7	7.06	94.2	900	33.0	91.0	83.5	87.2	83.7	83.7	88.2	7 00	. 00	90.5	97.2	0.96	2.66	102.5	100.0	103.5	04.2	010	6 00	3 6 6 6 6 1	7 00		٥٠٠ 8 م	88	77.5	76.0	73.5		110.5		124.4	
A 100		72.1	79.5	7.48	80.5		200	84.1	82.7	82.2	87.2	83.2	2,48	7 7		88.5	90.2	96.5	95.7	98.7	102.2	7.80	000	7 30		0.00	98.0	101.	7.66	89.1	88.7	78.0	76.7	74.2	•	109.5		122.6	
0110	ı	74.	79.	70		5,	8	84	83	23	8	מ	9 6	0 0	0 2	8 1	36	98	96	0 6	, ,	7 6		0.1	5	6	10	10	0	σ	6	7	_	76.5	•	110.5	•	122.8	
0.01	1	72.	77.		9 0	8	82	84.	83	C	70		0 1	3	8	88	90	66	0	9 0	0 0	203	, c	201	6	6	01	10	10	6	ō	α	0	010	_	1111.7	• • •	123.6	
	06.1	76.7	7 7 7	- 1	81.	90.5	86.2	85.0	2,0	ָ ה ה ה ה	0.70	2.08	84.0	85.0	88.	89.7	92.5	00,00		- 000	78.	104.	100.0	103.0	97.2	91.7	101.5	104.5	102.5	93.2	03.2	000	7 . 70	7.78	2.0		114.0	122.5	!
	140																																	83.0			112.0	121.4	1
	150		r. (	ت	Ŋ	Ŋ	^	ı ii	n i	n.	2	0	0	0	0	2		- 1	•	0	5	ပ	ပ္	• 5	3	0	0	7	7	-	- 1	• (	ۍ د	83.5	0.5		112.2	110 6	•
										_		ľ	400	c,	630		208	1000	1250	1600	2000	2500	3150	4000	000	7200				0000	2000	0000	5000	200	0000		_	PNL 10FT	₹0 <b>∨</b> E

107.8 109.6 110.2 109.9 110.5 109.4 112.0 114.0 115.0 116.1 115.3 114.9 110.2 102.7

FLYOVER

TABLE 11A

### PROP-FAN MCDEL/STCL WING NOISE DATA

0

CONFIGURATION- NO WING BLADE ANGLE-35.0 TIP SPEED-600.0

	150	140	130	120	110	100	A ZI MUTH 90	H ANGL	E (D	EG) 60	50	40	30	20	10
	œ	6	œ	80	ထီ	8	<b>.</b>	6	œ	<b>&amp;</b>	6	6	0	6	
63	62.0	62.0	62.0	61.2	62.0	62.2	62.5	62.7	62.0	62.2	62.5	63.0	64.0	70.5	
	9	5.	9	5.	ņ	6.	• 9	•	•	-	•	7.	œ	-	
0	-	•	6	5	Ş,	8	•	0	6	æ	Š	4.	4.	3.	
	Š	5	4.	ပံ	ငံ	6	S.	5	Š	4.	8	3	3.	3.	
9		0	-	-		ċ	-		ċ	-	0	-	2.	3.	
Ú	5	• 9	2	•	•	9	3	3	S	4	'n	5.	3	3	
S	4.	4.	ć	3	4,	3		S	Š	Ŋ,	Š	4	Š	4	
	9	6	ċ	6		~	7	<b>-</b>	-	8	<b>'</b>	-	8	8	
40	-	9	5	4.	5	5.	9	9	6.	7	• 9	9	÷	5.	
0	œ	5.	5.	5	9	Š	9	7.	о О	<b>ω</b>	8	œ	œ	•	
63	6	œ	ŝ	6	<b>&amp;</b>	~	æ	•	0	•	ċ	•	8	-	
80	ċ	ċ	ပံ	ထိ	œ	œ	6	0	0	<b>,</b>	<u>, , , , , , , , , , , , , , , , , , , </u>	-	6	-	
100	•	o	6	<b>&amp;</b>	7	φ.	6	-	• •	2	4	2	-	7	
125	3.	°	9	•	•	7	0	2.	-	3.	2.	3	2.	å	
160	5.	υ, •	ę	3	\$	2	4.	9	9	œ	<u>,                                     </u>	ò	5	-	
200	4.	4°	4.	2°	2	-	3.	9	<b>~</b>	ф Ф	<b>6</b>	7	Ş.		
250	œ	œ	å	9	9	5.	• 9	• 6	œ		-	ស		8	
315	5.	4.	4.	2.	2.	-	2	5	•	<b>ф</b>	8	6	9	2	
00	2	2		6	ဝံ	~	-	3,	5.	7	<u>~</u>	6	5.	,	
500	2		ô	6	œ	9	6		3	• 9	7	7	9	ċ	
30	4.	*	3	2.		6	7	4.	•	œ	Ġ	ċ	6	4•	
0	Š	2	* i	6	<b>~</b>	5.	• 9	-	2.	4.	'n	S.	Š	œ	
000	0	ċ	6	~	5	3	4.	<b>*</b>	ċ	2	'n	3	3	œ	
25C	3	2	<del></del> 1	°	æ	5	• 9	0		4.	Š	• 9	4.	-	
009	6	<b>~</b>	'n	4.	5	6	6	3	S.	-	6	ċ	~	-	
000		6	~	•	4.		-	5.	-	6	2	60	6	4	
500	3	2.	0	°		4.	4.	<b>~</b>	• Ф		'n	Š	<b>.</b>	Š	
20	8	7	-	5	3	•	•	3.	5	-	Ġ.	Ö	-	÷	
000	5.	5.	3	3.	%	ċ	•	-	m	ŝ	9	<u>~</u>	4•	-	
B (L	101.2	100.5	99.0	98.0	96.5	95.5	7.76	100.2	101.5	103.5	104.0	105.0	103.2	98.5	
10FT															
	•			0						. /	211	0 711	,	100	

110.5 109.0 109.2 107.5 102.0 106.0 107.0 109.2 107.7 111.5 112.2 112.7 113.7 108.0

116.3 118.3 120.1 118.2 118.8 118.8 120.8 122.3 121.1 124.2 123.0 122.0 119.8 112.0

DB(L) PNL 10FT FLYOVER

TABLE 12A

### PROP-FAN MCDEL/STCL WING NOISE DATA

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CONFIGURATION- NO WING BLADE ANGLE-35.0 TIP SPEED-801.0

							A ZI MUT	H ANG	LE (DE					
	150	140	130	120	110	100		0	<u></u>	09	20	04	30	20
90	8	~	0.59	· &	8	8	8	8	7	φ	7.	6	9.	6
	•	2	5	•	-	ċ	_;	2	• •	-		2	c,	*
	3	5.	'n	Š	4.	4.	4.	5	5	Š	3	S.	5	7
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$\sim$		-	2.	*	4.	3	•	6	ф 8	0	6	-	-	-
\$	8	7.	ပံ	2.	8	-	œ	3	-	4.	5	•	ŝ	3.
0	Š	9	•	•	7.	7.	-	œ	\$	œ	6	6	6	o
S	6	•	ငံ	ċ	ပံ	•		-	œ	<b>-</b>	-	2.	2.	5:
31	4.	9	ę,	4.	5	S	5.	5	3	5	'n	ŝ	5.	5
40	-	-	-	2	5.	8	2	3	•	8	<u>~</u>	2.	?	-
	7.67	81.5	2	83.7	83.2	82.7	83.7	84.7	81.0	84.7	84.0	83.5	83.5	83.0
63	4.	•	Š	J.	4.	4.	5	ŝ	2	5	5.	5	Š	4.
80	7	<b>~</b>	'n	4	4.	4.	5.	r,	2.	•	Ŷ.	• 9	•	4
100	7	Š	្ត	4.	ŝ	4.	ŝ	÷	'n	<b>.</b>	20	<b>α</b>	•	•
125	<b>&amp;</b>	7	<b>~</b>	•9	~	7	φ Φ	6	•	7	÷		ċ	<b>*</b>
160	010	6	ပံ	•9	ထို	\$	*	6	3	•	œ	6	ċ	<b>-</b>
200	°	å	တ္	\$		5.	3	<b>.</b>	3	œ	å	6	00	ç
250	88	8	۲,	8	٦,	ထိ	ô	, 2	6	3	G	3	3	ŝ
315	6	Ŝ	ŝ	• 9	5	Š	Š	6	7.	01.	<u>-</u>	03.	02.	5
400	6	9	\$	9	5	3.	• 9	00	œ	2	6 irru	m •	2.	• 9
00	2	å	'n	ထိ	8	œ	-	2	Š	07.	9	.90	. 90	• 1
30	4.	ŝ	ŝ	å	2	ô	Š	9	4.	<u>~</u>	6	6	6	4.
00	ô	φ.	ţ,	ထိ	۴	Š	7	0	8	<b>.</b>	4.	<b>*</b>	05.	ô
000	<b>*</b>	-	9	9	4°	3	4	٠,	5	•	÷	02.	03.	6
250	2.	, ,	ငံ	6	ထီ	9	<b>~</b> ~	0	7	Ξ,	3	05.	•	œ
00	9	9	•	4.	3		•	٠ ش	2	ŝ	۲.	6	000	2 •
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200	å	<u>.</u>	, <b>-</b> -		6	<b>∽</b>	• 9	• Ф	Š	6	2.	4•	Š	æ
150	<b>'</b>	• Ф	<b>~</b>	• 9	•	4.	3	4	\$	r.	ထိ	Ċ.	ċ	S
000	5	5	2	4.	3	e prod	2 •	3	0	4	÷	7	7	2

TABLE 13A

PROP-FAN MCDEL/STCL WING NOISE DATA

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_	BLADE ANGLE- 45.0	TIP SPEEN-598.0

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5.	<b>&amp;</b>	2.	6	7.	• 9	7	œ	• 	ċ	5	3.	4.	ŝ	ŝ	å	6	Š	-	-	œ	2	-	Š	5	6	-	4.	•	8		105.7	112.6	
0	S.	6	0	÷	Š	-	<b>&amp;</b>	=	•	2.	3	S.	-	Š	°	2.	<u></u>	ນໍ	04.	02.	Š	01.	00	01.	Š	œ	0	5.	2 •		110°C	120.0	
်	4.	8		<b>-</b>	Š	ъ Ф	6	-	•	'n	4.	5	7	<u>.</u> ۵	2	4	ç	4.	2	3	ŷ	i	φ.	2	5.	7	0	5.	Š		110.0	120.7	
6	3	<b>φ</b>	2	9	4•	•	-	0	•	3	5	5.	<u>`</u>	4.	2.	3	4.	<b>.</b>	04.	04.	Š	•	<b>œ</b>	•	3.	Š	œ	3	•		109.7	122.3	
6	3	œ	2	-	4.	<b>'</b>	<b>~</b>	<del></del>	-	3	5	v.	•	9	_	2	Š	'n	02.	01.	3.	œ	• 9	<b>-</b>	-	3	5	,i	• 6		108.0	121.4	
•	•	•	•	•	•	•	•	•	•		•	•	•	•	•	•		•	•	•		•	•	•	•	•	•	•		1	0.0	24.0	
•	•	•	•	•	•	•	•	•	•		•		•	•		•	•	•	•	•	•	•		•	•						J•0	24.1	
•	•		•	•	•		•		٠	•		•	•		•	٠				•	•			•	•		•		9	H	0.0	24.0	
•				٠	•	•																							•	5		23.6	
•	•	•	•	•		•	•		•			•			9	9					9			9						CHANNEL	0°0	22.9	
•	•	•	•	•	•	•		•	•				٠	•			•			•			•		•				0.0	VOICE	0.0	21.8	
•		•	•	•	•	•	•			•	•		9	•	•	•			•		•		•		4				•	H	•	20.5	
	•	•	•	•	•		•		•			•				*				•	•			•						AU TA	0.0	18.0	
			0	$\sim$	9	0	S	-	40	50	63	80	100	125	160	200	250	5	400	500	0	0	000	250	009	000	500	150	000		DB (L	10F Ynve	
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R0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0</td><td>50 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 59.5 59.2 60.0 60.7 65.2 78.  63 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 69.5 59.2 60.0 60.7 65.2 78.  8.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0</td><td>\$ 0.0 Start of the color of the color</td><td>50 0.C 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 O.C. 0.0 O.O. 0.0 O.O. 0.0 O.O. 0.0 0.0 0.0</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 0.C 0.C 0.C 0.C 0.C 0.C 0.C 0.C 0.C 0.</td></td></td>	50         0.0         0.0         0.0         0.0         0.0         60.0         77.2         77.2         77.2         77.2         77.2         77.2         77.2         77.2         77.2         77.2         77.2         77.2         77.2         76.7         77.2 </td <td>50         0.0         0.0         0.0         0.0         0.0         6.0         66.0         66.0         67.2         78.2<td>50         0.0         0.0         0.0         0.0         69.5         59.5         59.2         60.0         60.7         65.2         78.2           63         0.0         0.0         0.0         0.0         0.0         0.0         68.2         68.2         65.0         68.0         77.2</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50         0.0         0.0         0.0         0.0         6.0.0         66.0         68.2         78.2         67.0         68.0         79.5         78.2         68.2         68.2         68.0         68.0         77.2</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 59.5 59.2 60.0 60.7 65.2 78.  80 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 68.2 68.2 68.2 65.0 68.0 79.  80 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 63.7 64.2 65.0 60.7 65.2 78.  80 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 59.5 59.2 60.0 60.7 65.2 78.  81 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.</td><td>50 0.C 0.O 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0</td><td>50 0.C 0.0 0.0 0.0 0.0 0.0 0.0 0.0 59.5 59.2 60.0 60.7 65.2 78.  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TABLE 14A

### PROP-FAN MODEL/STCL WING NOISE DATA

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-	<b>~</b>	~	~	8	œ	80		6	6	6	6	0	-	4.	
_	9	• 9		7	•	œ	•	8	œ	6	ċ	•	•	4.	
œ	-		i	* }	ů	3		4.	3	ъ •	2	3.	3	4.	
œ	2.2	82.0	82.0	82.2	82.5	82.5	83.0	83.2	83.2	83.0	83.5	84.0	84.7	85.5	
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ထ	•	4	5.	5	4.	3.		5	4.	5	5	4.	4.	3	
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Ç	Ċ	6	ထိ	-	~	• 9		8	8	0	ċ	6	œ	Š	
Ç	3	2.	2.	• 	ငံ	ċ		2.	3	3	3	8	-	-	
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9	2.			ပံ	o°			4.	4•	• 9	Ŝ	Š	2	¢	
6	6	• 9	\$	• 9	<b>*</b>	-	•	<b>&amp;</b>	6	00	00	02.	æ	ŝ	
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01	1.5	3		6	6	å	•	4 •	Š	<b>~</b>	5.	9	6	ŝ	
	5,5	• 96	96	5	ů	Ŝ	•	6	03.	03.	02.	02.	•	4	
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	7.2	98	97.	97.	ş	5	•	œ	000	01.	03.	03.	<b>~</b>	ŝ	
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	7.5	• 96	•	•9	4.	2	•	ω •	5.	7	6	9	-	<b>œ</b>	
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$\infty$	, , ,	6	6	6	7.	4.	•	4	5	~	œ	<b>ф</b>	3	-	
~	œ	å	7		Š	3	•	3.	4.	5	• 9	•	3.	e rant	
01	9.5	110.0	108.5	108.2	107.2	107.0	108.0	110.2	111.2	113.5	112.7	113.0	107.5	104.7	
	,	•		(		•	;		ć	U	ŗ	ć	*		
<del>-</del>	2.0	7.611	119.3	1 1 % 4 T	11 % 1	114.8	171.4	1.5.8	174.3	0.621	7.671	122.0	114.0	10801	

114.1 117.7 118.5 118.2 117.5 118.0 119.9 121.5 123.4 123.0 122.1 120.6 113.0 106.6

PNL 10FT FLYOVER

TABLE 15A

### PROP-FAN MCDEL/STCL WING NOTSF DATA

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WING CON FIGURATION— ND BLADE ANGLE— 50.0 TIP SPEED—599.0

140	130	120	110	100	A ZI MUTH 90	ANG 80	LE_ (DE 70	EG) 60	20	40	30	20	10
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63.0		62.7	63.7	63.2	62.5	63.7	63.5	64.7	64.5	66.5	69.5	82.7	
9		-		-	~	•	φ	œ	6	0	4	2	
6		Š	4	8	ċ	•	~	0	8	<u>-</u>	8	2	
Š		3	3.	5.	7.	•	φ	7	9	Š	<b>~</b>	•	
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ů		4.	8	<b>ө</b>	7	•	ထ	-	œ	<b>ө</b>	¢.	ċ	
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'n			-	2.	-	•	2.	٠.	2	2.	2.	2.	
o		-	•	•		•	2.	2	2	2.	-	-	
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-		•	4.	3	5	•	•	7	5	•	5.	3.	
-		5.	Š	•	5.	•	7	<u>~</u>	7	7.	5.	3	
7		•	9	•	7	•	œ	6	6	6	-	2	
φ,		4.	7.	-	• 9	•	6	-	5.	4.	3.	œ	
5			-		2	•	4.	4.	4.	2.	ċ	•	
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'n		3	3,	6	2.	•	9	•	9	-	4	2	
3.		2.		¢	-		ŝ	3	6.	7.	2.	6	
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2.		2	ငံ	ò	-	•	Š	-	-	۲.	3	ò	
6		å	~	9	• 9	•	ċ	02.	02.	03.	<b>.</b>	2.	
9		Š	4.	2.	4	•	ф Ф		-	-	•	5	
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5		4	-		0	•	2	5	9	•	•	ŝ	
<b>!</b>		,	'n.	3	2.	•	4.	>	φ,	å	2.	7	
2.		ċ	8	9	5	•	9	0	-		5.	ċ	
<b>~</b>		• 9	5	2	•	•	٠,	• 9	<b>~</b>	-	•	7	
5.		4.	2.	°.	6	•	-	ί,	4.	4.	<b>6</b> .	•	
107.0		106.7	105.0	104.7	105.5	107.7	110.0	111.0	1111.0	1111.0	105.7	102.2	

116.5 121.1 121.6 120.6 121.6 120.7 122.3 123.5 124.7 124.9 125.4 122.3 115.8 108.6

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TABLE 16A

### PROP-FAN MCDEL/STCL WING NOISF DATA

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CONFIGURATION— NO WING BLADE ANGLE— 50.0 TIP SPEED—641.0

			H ANG	(DE	(9				
140 130 120 110	10	0	80	10	09	20	40	30	20
8.2 68.0 68.7 6	9	.7 68.	67.	œ	80	æ	6	•	E.
1.5 71.2 71.7 7.	7.1	.7 71.	72.	2	2	2.	2.	4.	\$
4.5 75.5 75.5 7	75	.5 75.	75.	ŝ	•	5.	-	7.	4.
3.7 83.2 83.0 8	.7 84	.5 84.	84.	<b>ω</b> .	4.	5	3.	4.	9
88.2 85.0 83.7 87	.7 90	3.2 90.5	89.2	87.5	84.5	84.0	0.98	87.2	87.5
7 2.67 79.0 79.2 7	.0 79	.2 79.	79.	6	•	0	-	2.	4.
6.5 76.7 77.5	.7 78	.5 79.	80.	0	_		-	2	3
0.5 80.0 80.0	2.0 84	.0 84.	86.	9	<b>-</b>	• 9	9	ŝ	Š
5.2 85.5 86.0	5.5 86	.2 87.	86.	5	• 9	•	. 9	• 9	•
1.7 82.7 84.C	3.2 83	.7 85.	84.	4	ۍ. •	4•	4	4.	4
5.2 86.2 86.0	4.2 84	.7 85.	85.	5	• 9	•	• 9	5	m
9.0 88.5 86.7	6.0 87	.2 88.	87.	<b>-</b>	œ	æ	-	•	2
9.5 87.5 86.2	7.5 87	.0 87.	88	ф Ф	œ	6	6	-	4.
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5.2 95.0 95.2	.7 91	• 5 96 •	93.	2.5	000	-	6	3	ċ
5.2 95.7 96.0	.7 93	.0 97.	95.	8.5	ô	7	6	4	•
3.5 93.5 92.7	.2 93	• 96 0•	• 96	7.2	98.	8	• 9	3	6
4.5 94.2 93.2 9	.2 91	.5 92.	• 96	<u>~</u>	6	00	7	Š	2.
5.5 95.7 94.2 9	.7 92	.7 94.	97.	7.5	66	01.	6	• 9	2
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0.5 100.0 99.2	8.2 98	•66 0•	101	0.40	05.	0.20	0.5	6	'n
5.5 96.2 95.7	5.2 95	.5 96.	97.	0.00	02.	0.20	01.	•	ď
1.7 101.2 100.7	9.0 97	.7 99.	101.	03.0	04.	05.5	0.5	6	4.
7.5 97.7 97.0	5.7 94	.5 96.	98	00.5	02.	03.5	03.	-	4.
1.5 101.2 100.5	9.5 97	.5 99.	100.	05.0	04.	05.5	05.	8	3
7.2 97.0 96.0	.5 92	.0 93.	• 46	6.	<u>,</u>	6	6	2	<b>;</b>
9.7 89.5 89.0	.0 84	.2 84.	86.	<u>~</u>	6	7	-	Š	6
3.7 83.7 82.5	.5 77	.7 78.	78.	0	2	6	3	-	ന
0.0 86.2 79.0	.5 74	.7 74.	75.	•	ထ	6	6	4.	-
8.0 77.5 76.0	0.5 72	.7 73.	73.	5	9	7.	-	3.	ċ
10.5 109.5 109.0 10	08.0 107	7.0 108.5	109.5	1111.0	113.0	113.5 1	13.0	108.0	104.5

Hamilton	U
Standard	DIVISION OF UNITED AIRCRAFT CORPORATION

HSER 5910

#### APPENDIX B

DATA ACCURACY CONSIDERATIONS



#### INTRODUCTION

The Prop-Fan/STOL Wing test data is unique in that the test item is a simple aerodynamic configuration, the test environment is close to ideal, and a range of operating conditions were tested. In order to make the data from this program useful to other acoustic investigators, an analysis of the accuracy of the data presented has been conducted. This analysis which is summarized below includes evaluation of: (1) measurement and analysis system frequency response, (2) averaging time during data reduction, and (3) influence of total background noise on the test data.

#### SYSTEM FREQUENCY RESPONSE

Prior to testing, the CEC VR3300 tape recorder frequency response was determined by recording oscillator signals at various frequencies from 100 to 40 KHz at a constant input voltage and playing back on the Hamilton Standard data reduction system. Since both the narrow band and one-third octave band analyzers used for data reduction were limited to 20 KHz, the test data was played back at one-half the tape speed used during recording to allow analysis to 40 KHz. Consequently, the frequency characteristics were determined at 7 1/2 ips. Figure 1B shows the frequency response. Since the microphone of interest required a nose cone windscreen to reduce wind noise in the Prop-Fan wake, it is therefore necessary to consider the microphone/windscreen response at zero degree incidence. This response, as shown on Figure 2B, falls off rapidly from 15K to 20 KHz. Past 20 KHz the response is unpredictable due to standing waves between the nose cone housing and the microphone diaphragm. It should be noted that the data presented has not been corrected for this variation in frequency response.

#### DATA REDUCTION AVERAGING TIME

In analyzing the sweep data, which was recorded from a microphone traversing at approximately 0.5 degree per second, it was necessary to select an averaging time which would minimize the statistical error without sacrificing the directional character of the data.

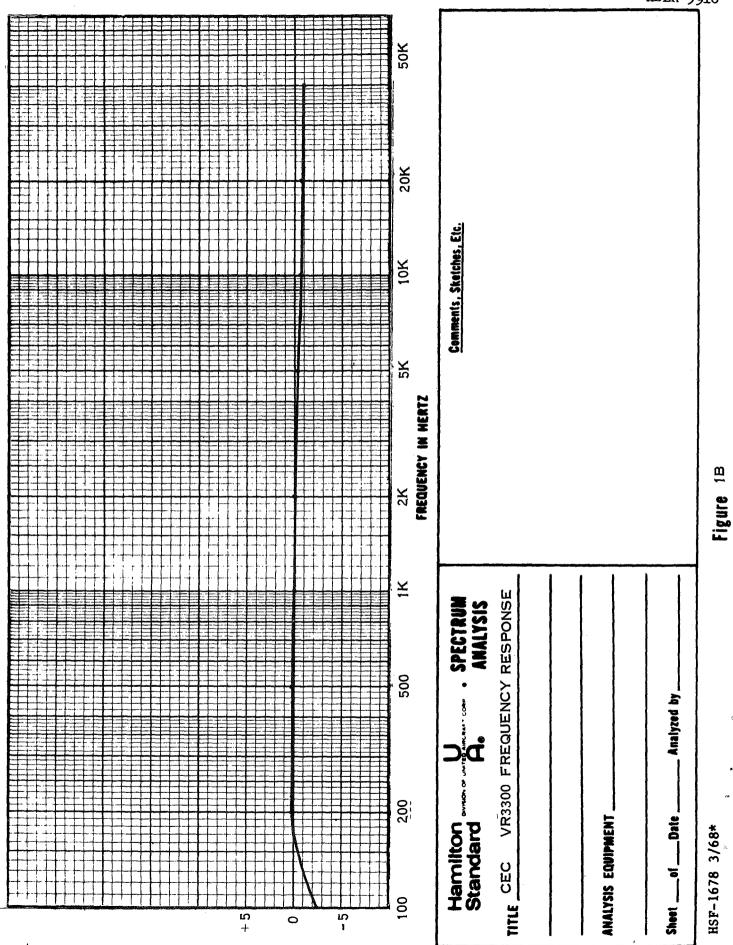
For the data reduction using one-third octave filters, an averaging time of four seconds was selected to facilitate data reduction while minimizing statistical error. In order to determine this error, a single four-minute stationary data point was analyzed continuously using a four-second averaging time. The results, as shown on Figure 3B, indicate the spread of data to be 3 dB or less in all but one of the one-third octaves considered. In like manner, an averaging time of 0.5 second was chosen for the narrow band (40 Hz constant bandwidth filter) analysis.

#### TOTAL BACKGROUND NOISE

Prior to each set of tests, background noise measurements were made at various input gain settings of the tape recorder signal conditioners, for each microphone. These recordings, when played back through the data

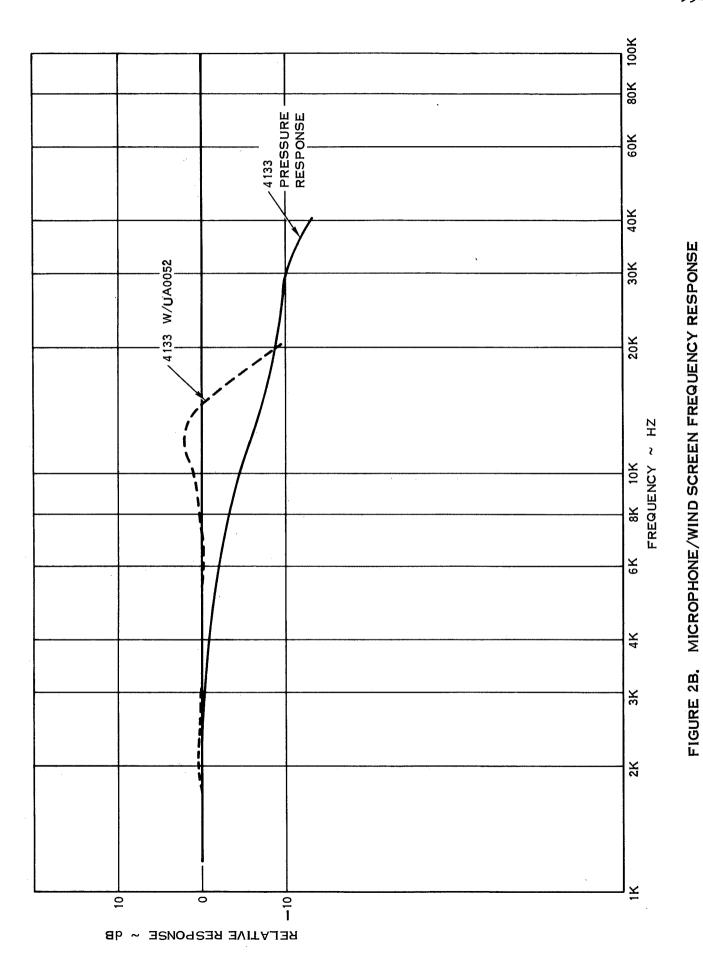


reduction system, include ambient acoustic noise as well as the electrical noise of the recording system, playback system, and analyzer system. These total background noise levels are shown on each of the narrow band curves of Figures 27 through 29.



RELATIVE SOUND PRESSURE LEVEL db re .0002  $\mu$  bar

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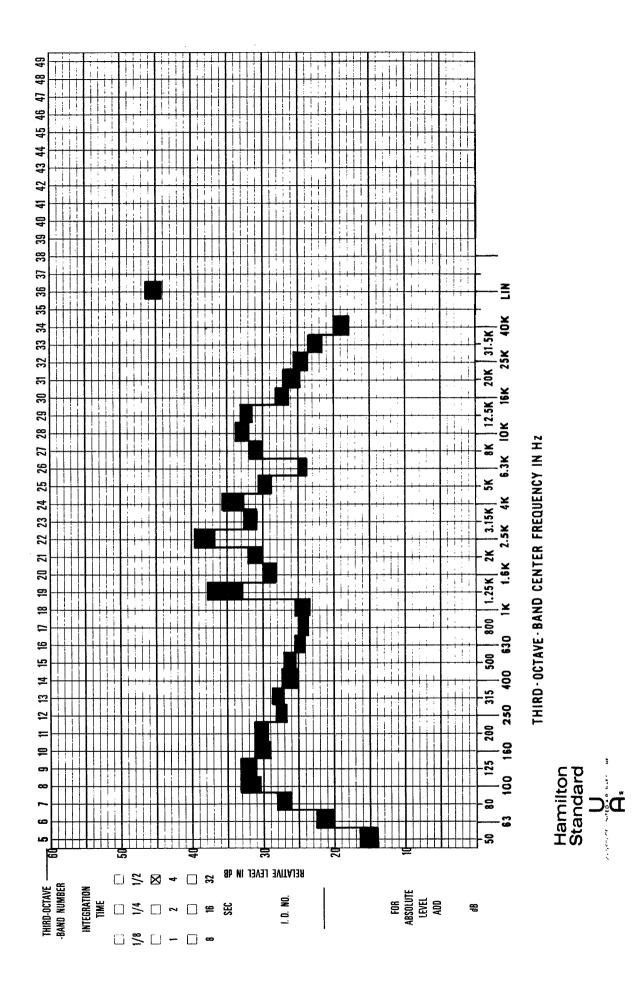


FIGURE 3B PROP-FAN/STOL WING NOISE VARIANCE

THIRD-OCTAVE-BAND ANALYSIS Hamilton U Standard OF UNITED AIRCRAFT CORPORATION A®

APPENDIX C

REFERENCES

Hamilton
Standard

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